

CATALYST LAYER MODELING: THE NEXT GENERATION

Further FC Workshop, DLR Stuttgart, July 6, 2022

Michael Eikerling, Institute of Energy and Climate Research, IEK-13

Further Understanding
Related to Transport
limitations at High
current density towards
future ElectRodes for
Fuel Cells



WHAT CAN BE LEARNED FROM EXISTING MODELS?

LOW PT LOADING: WHAT IS TIPPING THE BALANCE?

RATIONALIZE WETTING BEHAVIOUR IN CCL

IMPORTANCE OF CROSS-COMPONENT COUPLING



HELMHOLTZ RESEARCH FOR
GRAND CHALLENGES



Funded by
Federal Ministry
of Education
and Research



WHY THEORY AND COMPUTATION?

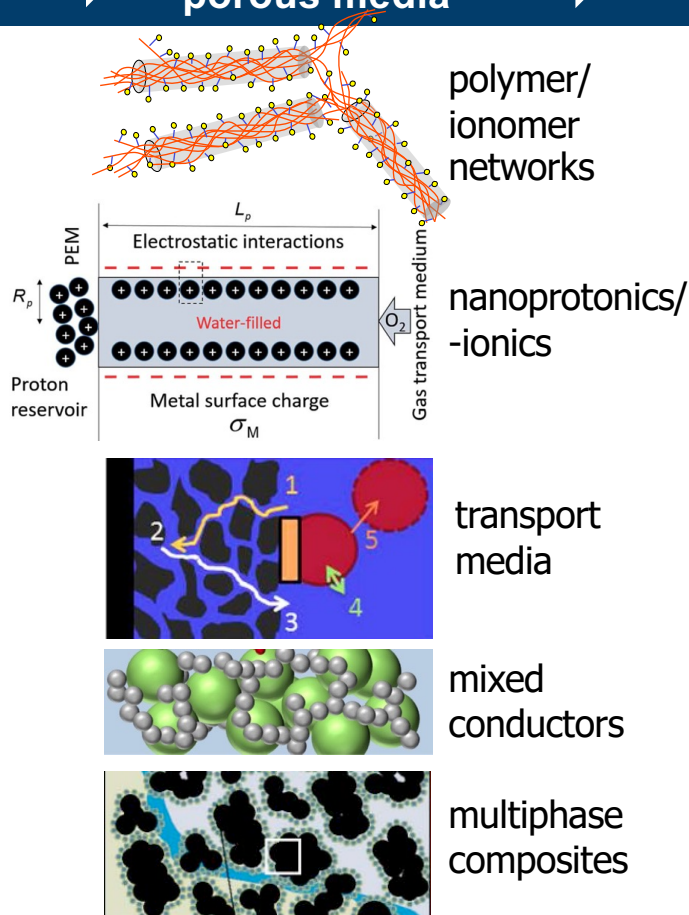
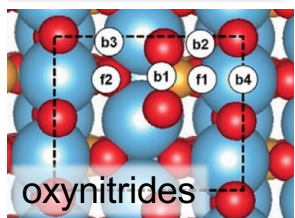
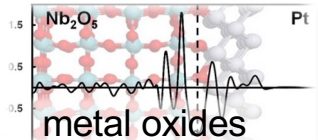
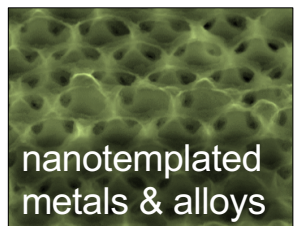
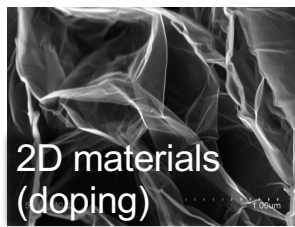
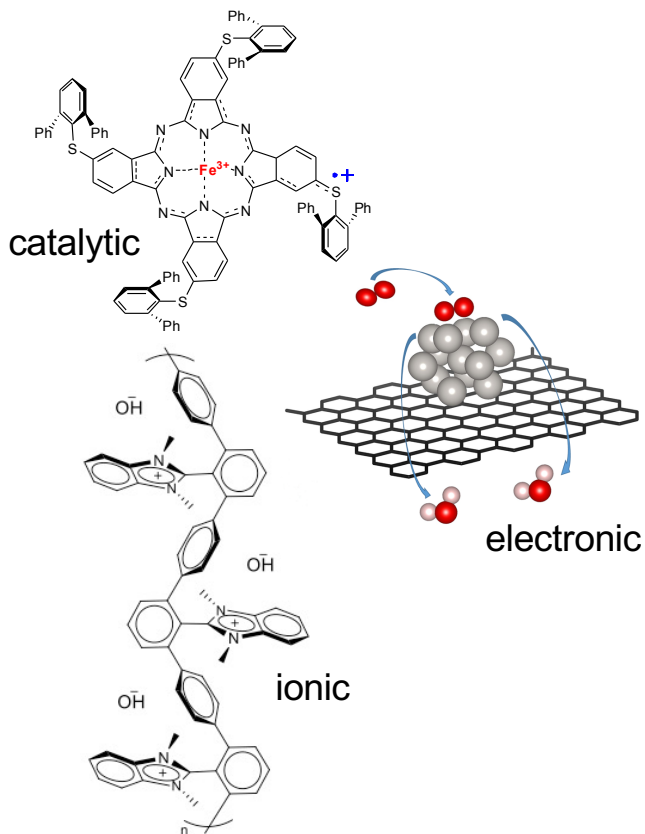
Molecular & atomistic design



Structured materials & interfaces



Composites & porous media



BATTERY ENERGY STORAGE



HYDROGEN FOR MOBILITY



CHEMICAL ENERGY STORAGE AND CCU



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Michael Eikerling, IEK-13: Theory and Computation of Energy Materials

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WHY THEORY AND COMPUTATION?

Molecular & atomistic design



Structured materials & interfaces



Composites & porous media



BATTERY ENERGY STORAGE



AI-BASED DESIGN

DEVICE LEVEL → do properties meet use-specific demands (technology as driver)?

→ **METRICS**

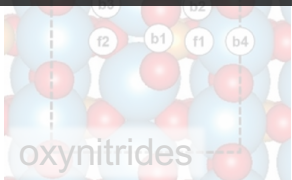
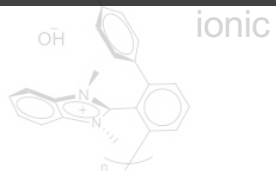
MACROSCALE → mixed (“multi”) functionality

MESOSCALE → interfacial phenomena

MICROSCALE → transfer of energy, charge, and matter

INTRINSIC → mechanical, thermal, electronic, ionic, electrostatic, catalytic etc.

↑
DESCRIPTORS

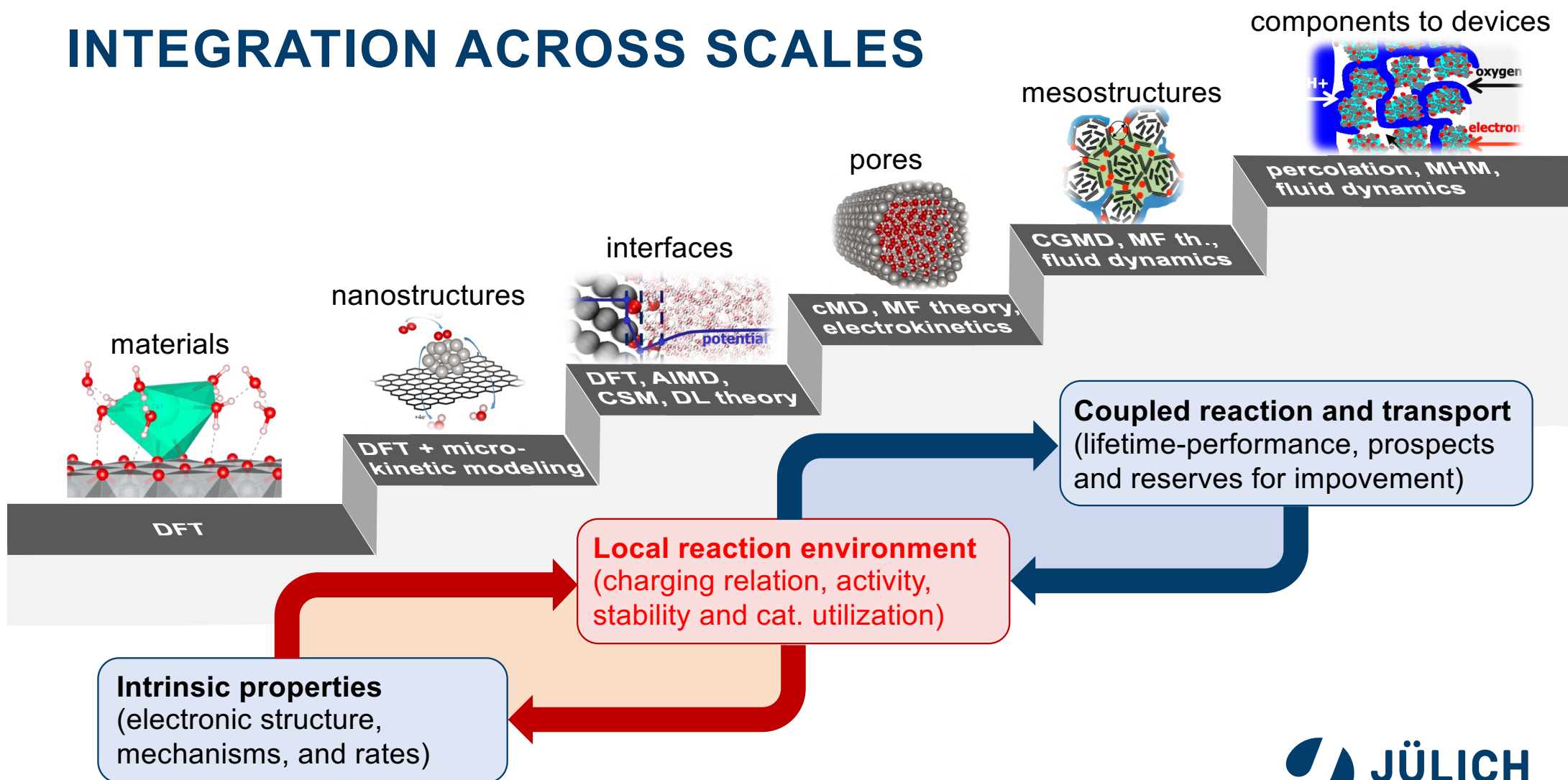


conductors
multiphase composites



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INTEGRATION ACROSS SCALES



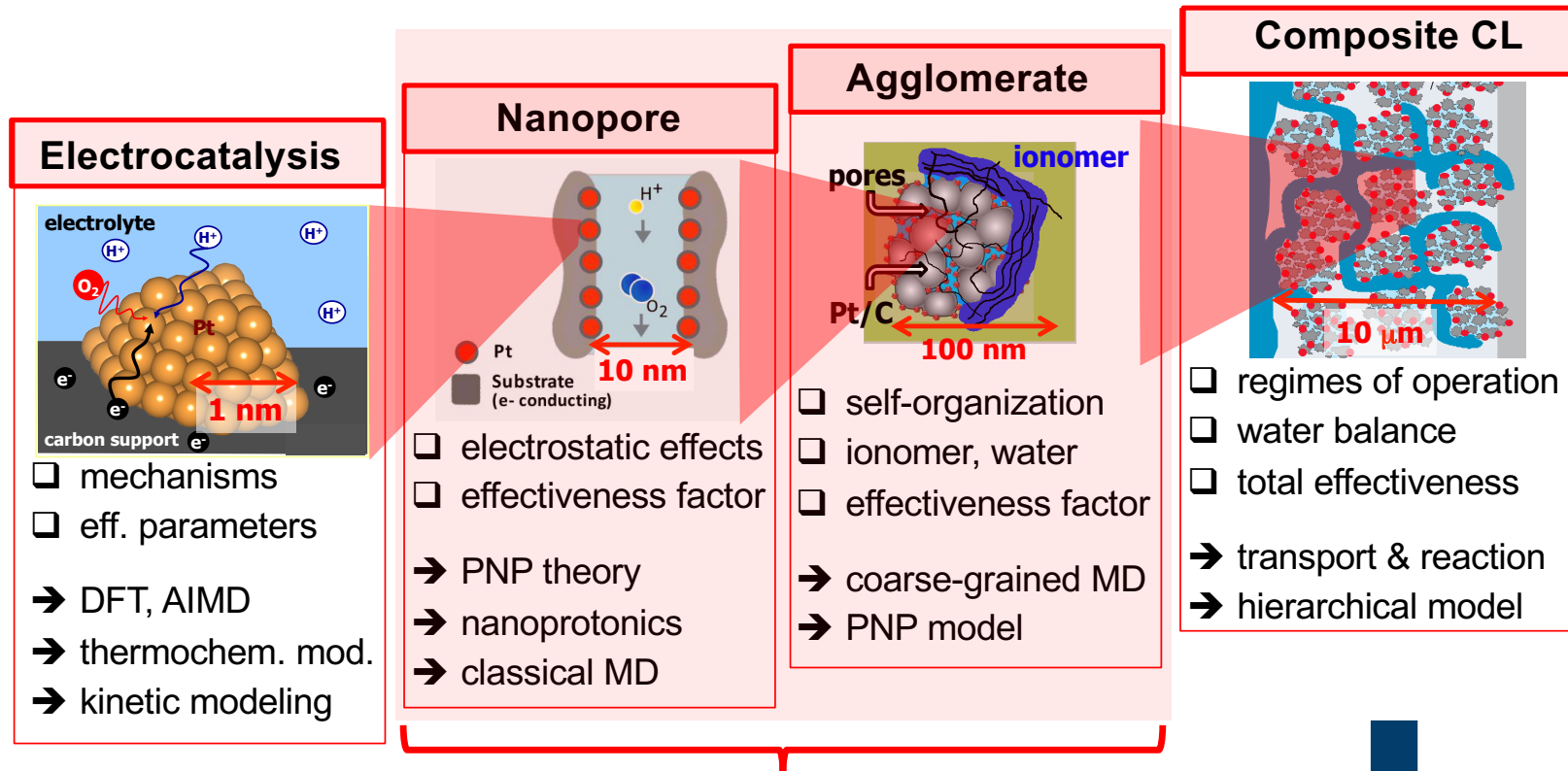
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LOCAL REACTION ENVIRONMENT: COUPLING



- mechanistic understanding
- material selection & design
- key electrode parameters

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local reaction environment

transport

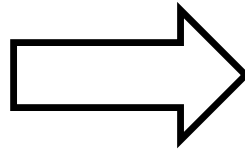
nonuniformity

**STRUCTURE-BASED MODELING OF CATHODE
CATALYST LAYERS IN PEM FUEL CELLS**

FROM COMPOSITION TO EFFECTIVE PROPERTIES

Primary parameters

- ❑ component densities: $\rho_{Pt}, \rho_C, \rho_{el}$
- ❑ weight fractions: Y_{Pt}, Y_{el}
- ❑ Pt mass loading: m_{Pt}
per geometric surface area
- ❑ layer thickness: l_{CL}

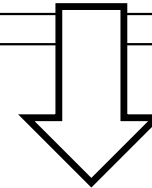


Volumetric composition

$$X_{Pt} = \frac{m_{Pt}}{l_{CL}} \frac{1}{\rho_{Pt}},$$

$$X_C = \frac{m_{Pt}}{l_{CL}} \frac{1 - Y_{Pt}}{Y_{Pt} \rho_C},$$

$$X_{el} = \frac{m_{Pt}}{l_{CL}} \frac{Y_{el}}{(1 - Y_{el}) Y_{Pt} \rho_{el}}$$



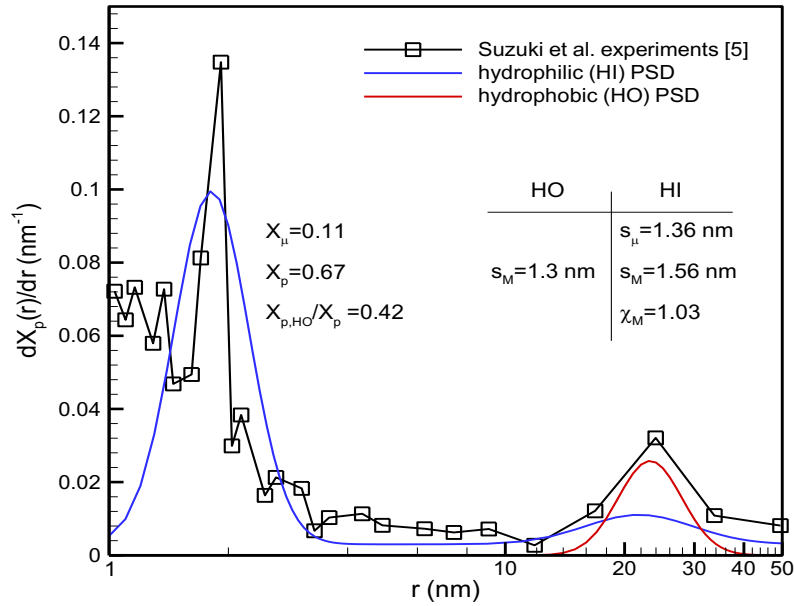
Effective properties from percolation theory

$$\sigma_{el} = \sigma_0 \left(\frac{X_{el} - X_c}{1 - X_c} \right)^\mu \Theta(X_{el} - X_c)$$

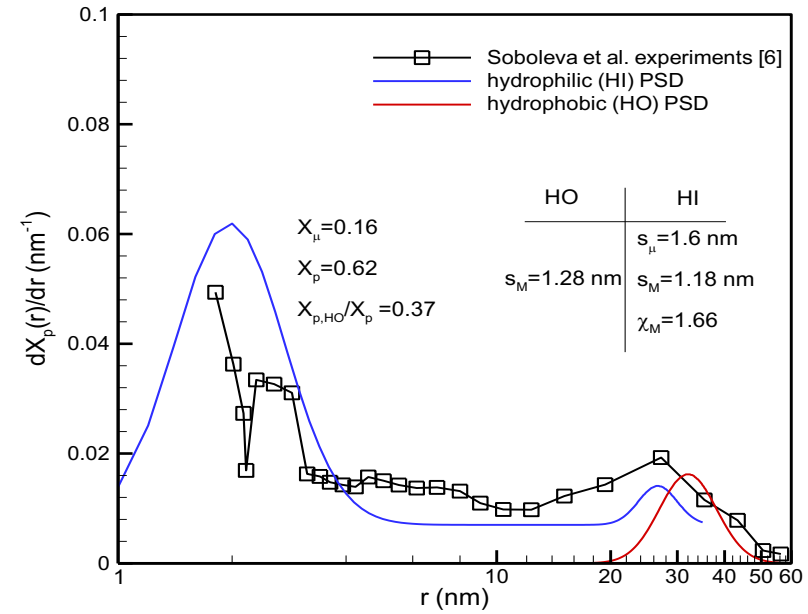
$$D^{o,v,r}(S_r) = D_0^{o,v,r} \frac{(X_P - X_\mu - X_c)^{2.4}}{(1 - X_c)^2 (X_P - X_c)^{0.4}} \left\{ \left[\frac{(1 - S_r) X_P - X_c}{X_P - X_\mu - X_c} \right]^{2.4} \Theta \left(S_r - \frac{X_\mu}{X_P} \right) + \Theta \left(\frac{X_\mu}{X_P} - S_r \right) \right\} + D^{res}, \quad D_0^{o,v} = \sqrt{\frac{2RT}{\pi M^{o,v}}} \frac{4}{3} r_{crit}$$

$$j^0 = j_*^0 \frac{m_{Pt} N_A}{M_{Pt} \nu_{Pt}} \Gamma_{np} \Gamma_{stat}, \quad \Gamma_{stat} = g(S_r) \frac{f(X_{PtC}, X_{el})}{X_{PtC}}$$

EXPERIMENTAL PORE SIZE DISTRIBUTIONS



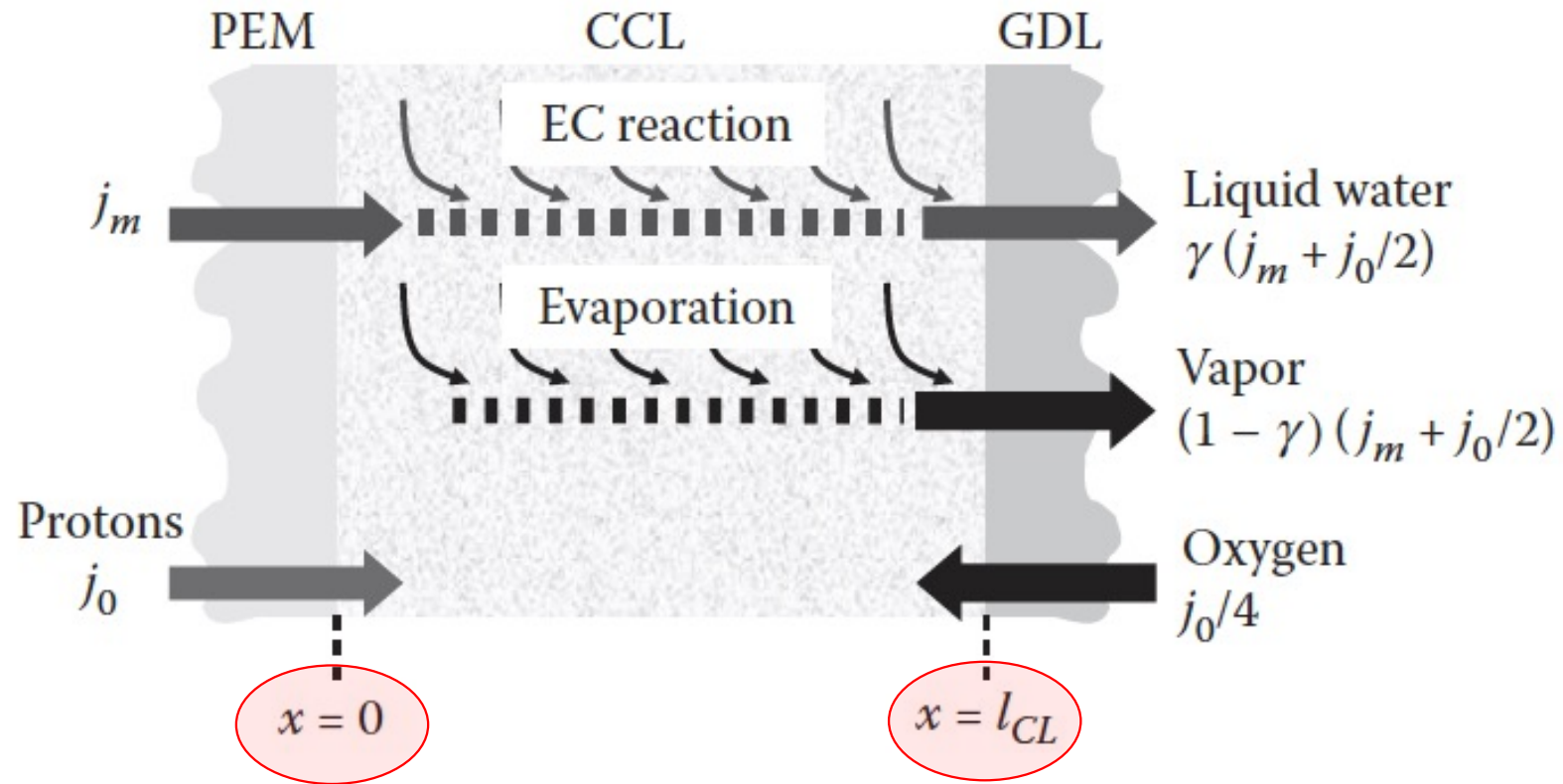
T. Suzuki *et al.*, Int. J. Hydrogen Energy, 36, 12361 (2011).



T. Soboleva *et al.*, ACS AMI, 2, 375 (2010).

- bimodal pores size distribution (→ agglomeration)
- hydrophobic and hydrophilic pores

COUPLED SPECIES FLUXES IN CCLS



MHM: COUPLING

Part A: Governing equations for electrochemical processes

Proton transport $\frac{d\eta}{dx} = \frac{j_p(x)}{\sigma_{el}(S(x))}$

Interfacial reaction $\frac{dj_p}{dx} = -Q^{ec}(x)$

Oxygen diffusion $\frac{dp}{dx} = \frac{j_0 - j_p(x)}{4fD^o(S(x))}$

explicit
coupling

Part B: Governing equations for water fluxes

Water formation and vaporization $\frac{dj^l}{dx} = \frac{1}{2}Q^{ec}(x) - Q^{lv}(x)$

Liquid transport $\frac{dp^l}{dx} = \frac{1}{B_0 f K^l(S(x))} \left[\left(n + \frac{1}{2} \right) (j_p(x) - j_0) + j^v(x) + nj_0 - j_m \right]$

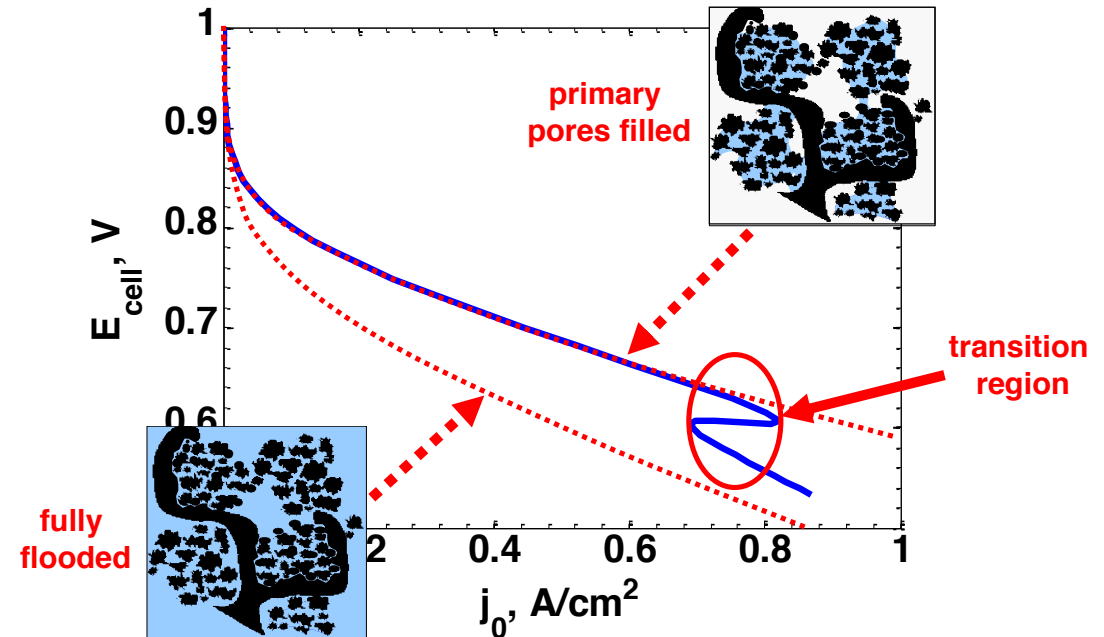
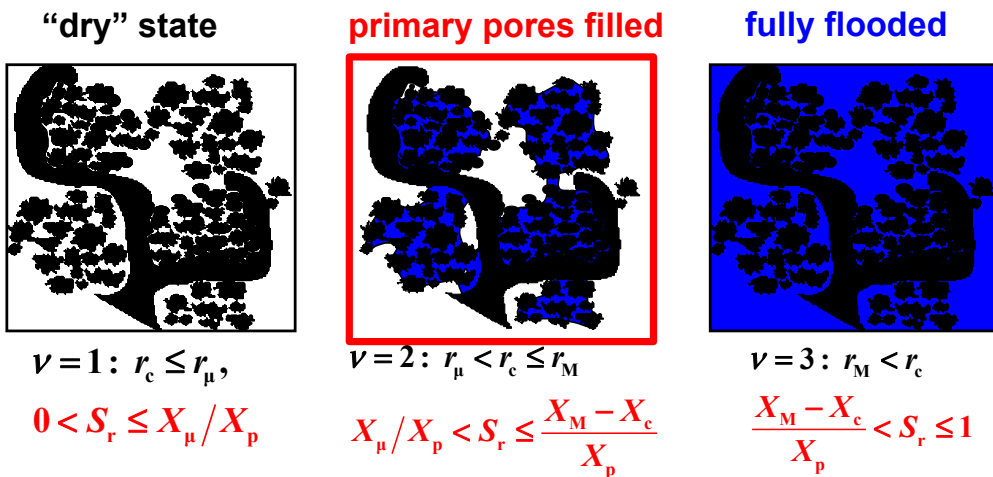
Vaporization exchange $\frac{dj^v}{dx} = Q^{lv}(x)$

Vapour diffusion $\frac{dq}{dx} = -\frac{j^v(x)}{fD^v(S(x))}$

Problem: implicit coupling –
dependence of solution on $S(x)$

Polymer Electrolyte Fuel Cells – Physical Principles of Materials and Operation, M. Eikerling and A.A. Kulikovsky, CRC Press, 2014.

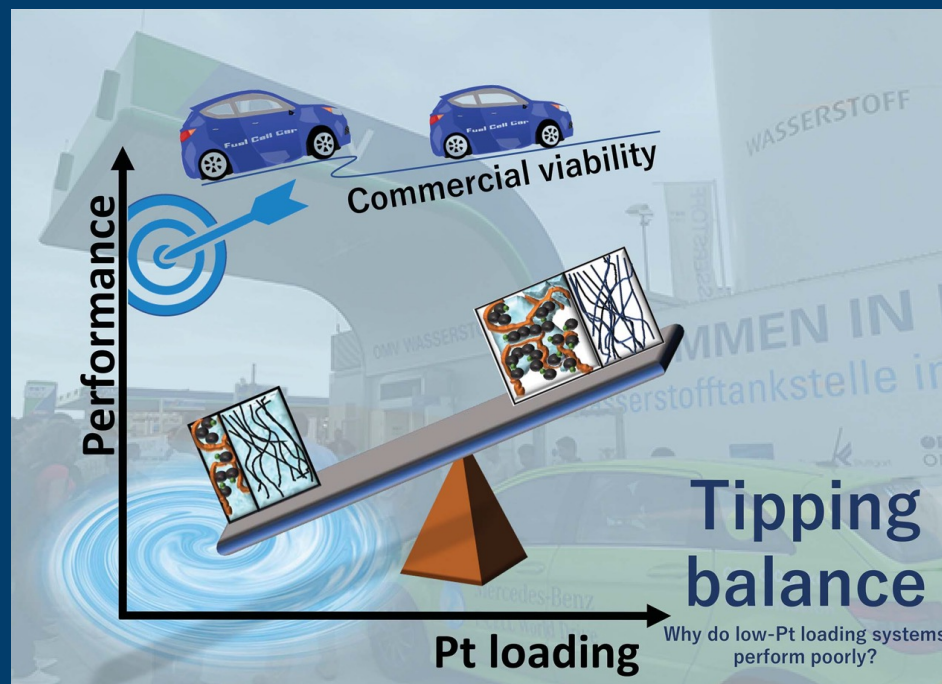
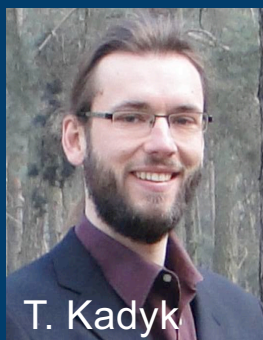
WHAT HARM CAN A FLOODED CCL POSSIBLY DO?



- ❑ important impact: thickness, composition, pore size distribution, wettability
- ❑ assumption of constant composition sufficient below transition region

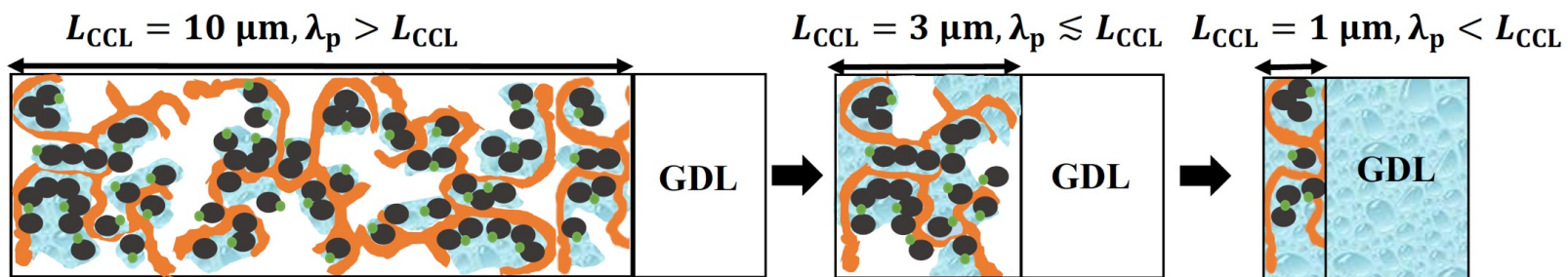
CCL flooding: important, but not critical! A flooded electrode could still perform well.

CCL WITH LOW PT LOADING: WHAT IS TIPPING THEIR PERFORMANCE?

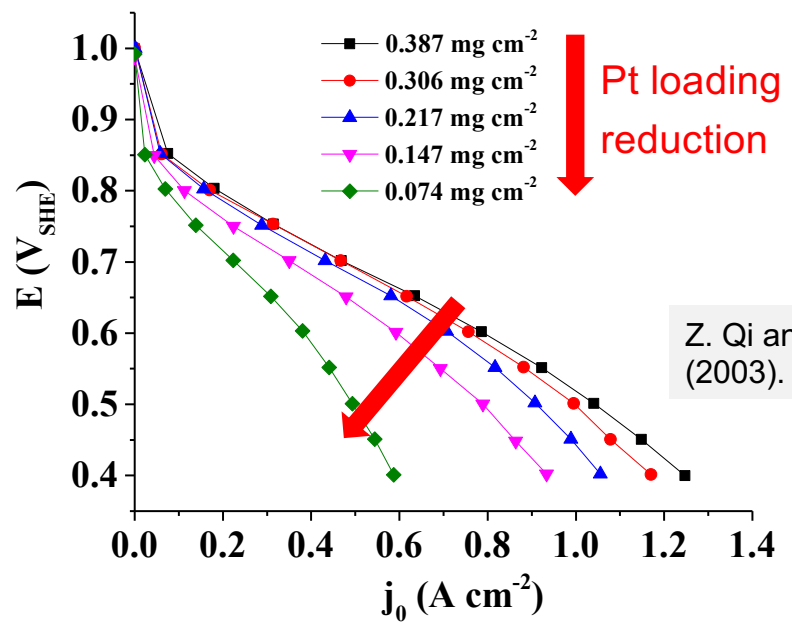


T. Muzaffar *et al.* (2018). *Sustainable Energy Fuels* 2, 1189-1196.

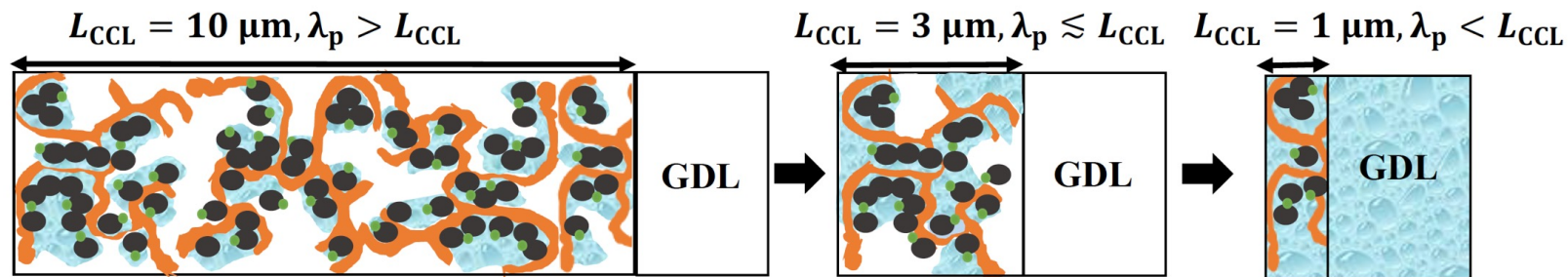
CATALYST LAYERS WITH REDUCED PT LOADING



13 studies analyzed (1992 to 2016),
i.e., fitted with performance model.

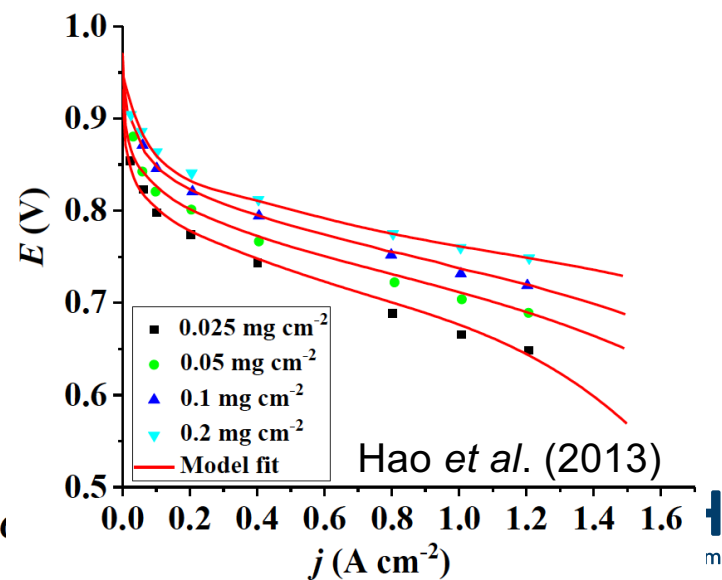
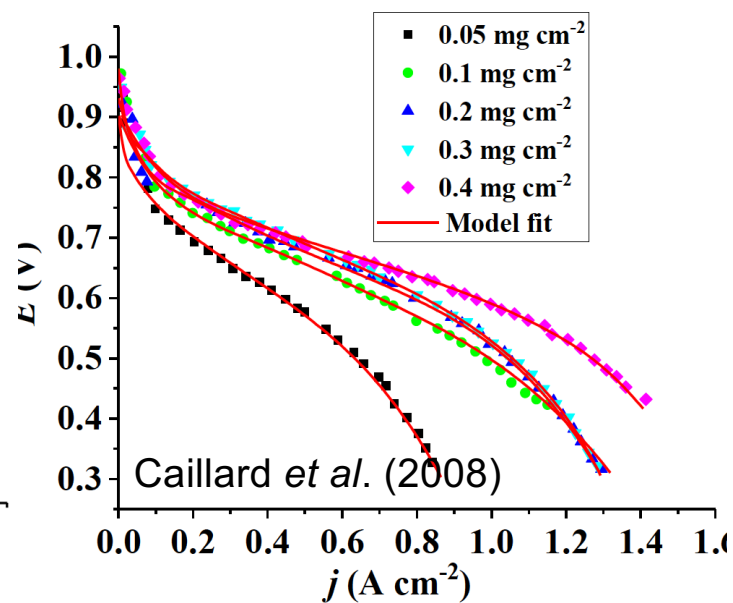
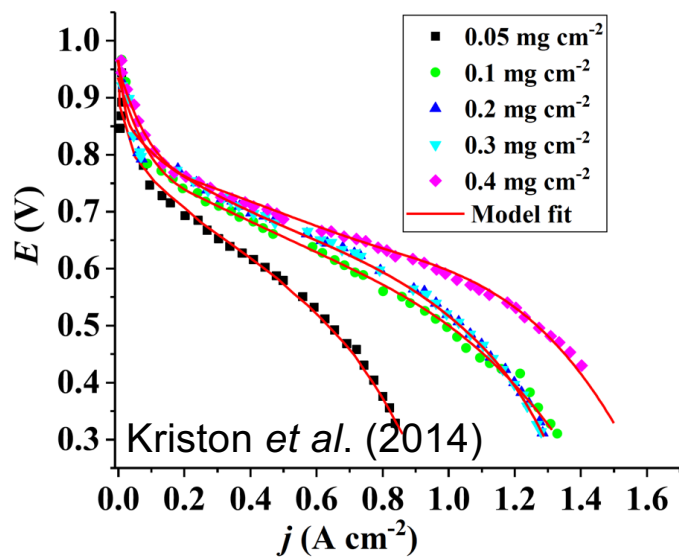
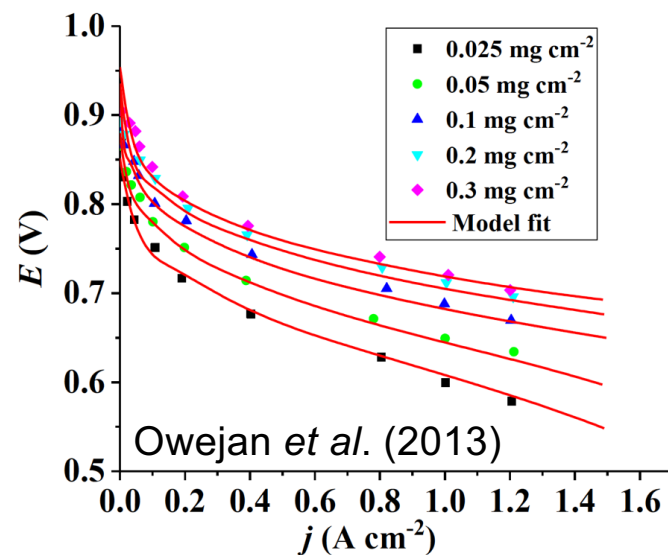
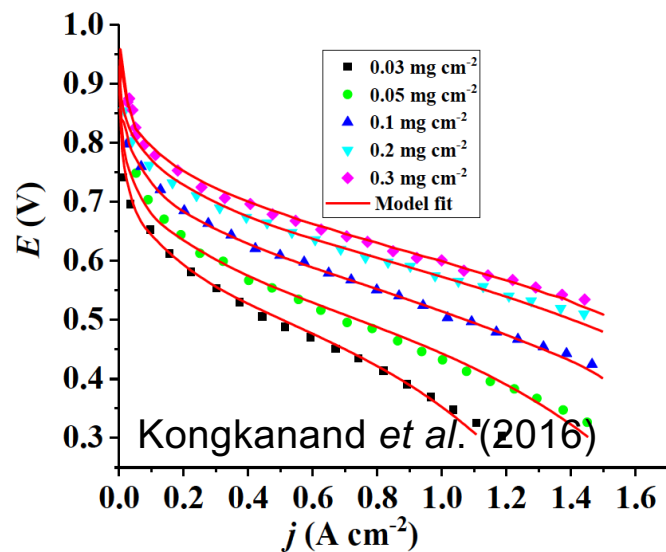
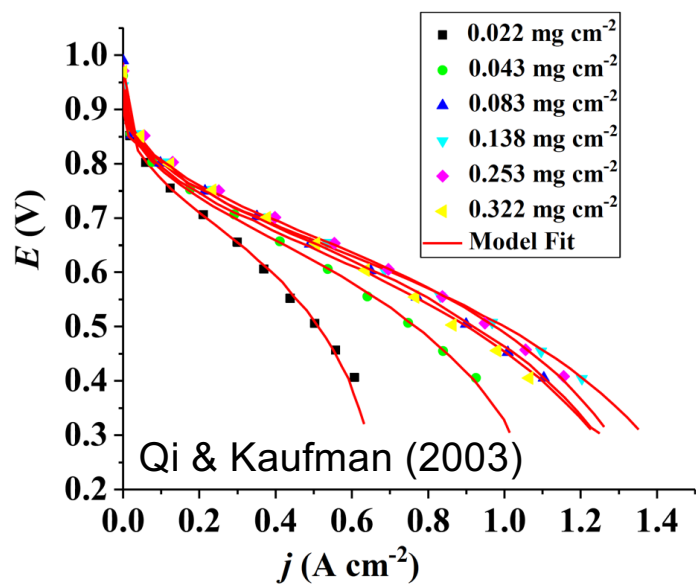


CATALYST LAYERS WITH REDUCED PT LOADING



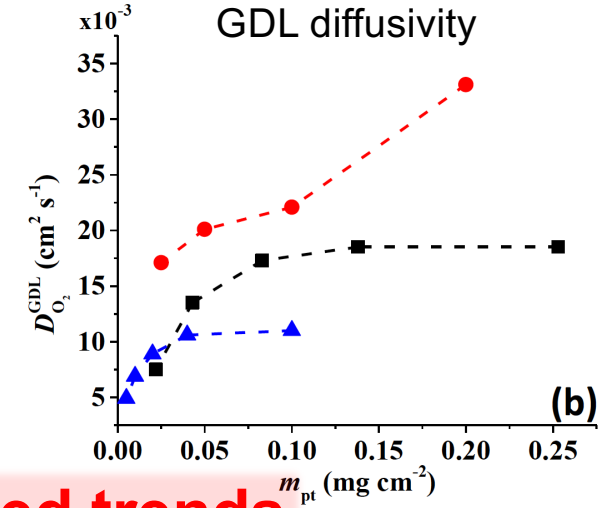
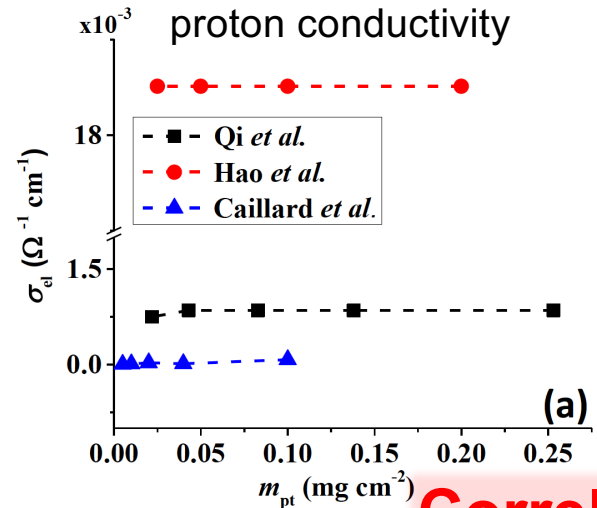
Thickness reduction (at fixed current density)

- increased rate of water production per unit volume
- loss of volumetric vaporization capability
- larger proportion of liquid water flux from CCL
- **flooding of GDL**
- **oxygen diffusion inhibited**

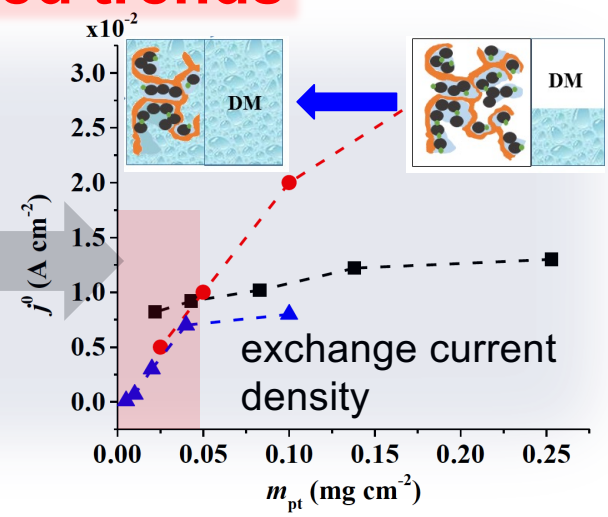
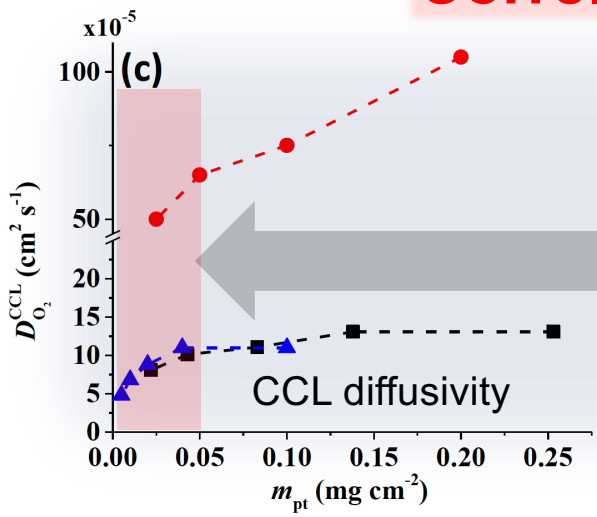


VARIATION OF PROPERTIES WITH PT LOADING

ionomer-based CCLs should not be too thin → **“forbidden”** thickness range



Correlated trends



T. Muzaffar *et al.* (2018). Sustainable Energy Fuels 2, 1189-1196.

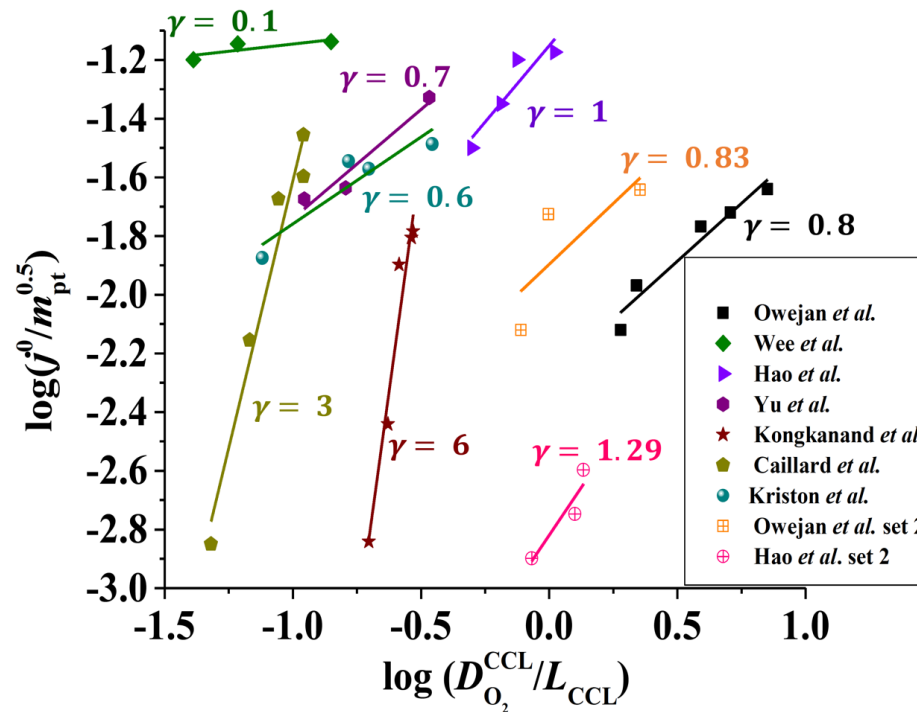
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Michael Eikerling, IEK-13: Theory and Compu

VARIATION OF PROPERTIES WITH PT LOADING

Correlation analysis based on porous electrode theory

$$j_{\text{eff}}^0 = \frac{2(m_{\text{Pt}} j_*^0 \delta)^{1/2}}{j_0} \left(\frac{4Fp_{\text{O}_2}^0}{RT} \right)^\gamma \left(\frac{D_{\text{O}_2}^{\text{CCL}}}{L_{\text{CCL}}} \right)^\gamma$$



Well-designed layer:

$0 \leq \gamma \leq 0.5$
 ↑ ideal utilization
 ↑ power performance

T. Muzaffar *et al.* (2018).
 Sustainable Energy Fuels 2,
 1189-1196.

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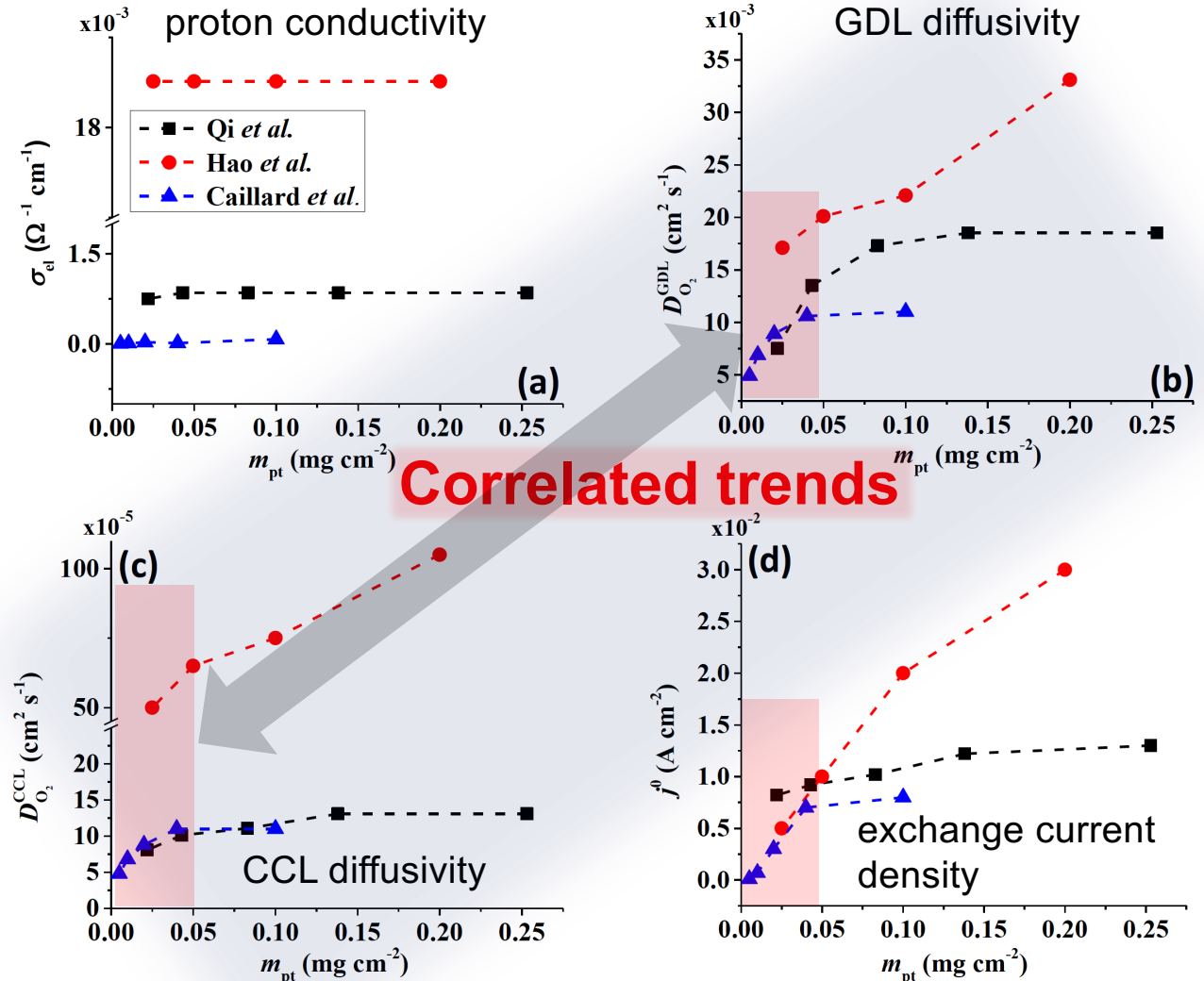
Michael Eikerling, IEK-13: Theory and Computation of Energy Materials

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VARIATION OF PROPERTIES WITH PT LOADING

CCL flooding triggers GDL flooding → origin of dramatic decline in performance?



T. Muzaffar *et al.* (2018).
Sustainable Energy Fuels 2,
1189-1196.

MODELING MICROSTRUCTURE FORMATION AND WETTABILITY EFFECTS IN CCL



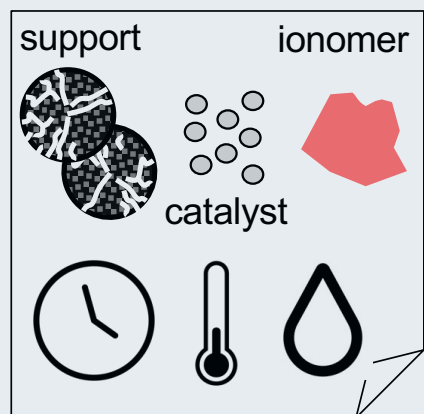
Wolfgang



MODELING MICROSTRUCTURE FORMATION IN CCL

Prediction of volumetric composition and ionomer film thickness and coverage based on ink recipe

Ink recipe & fab conditions



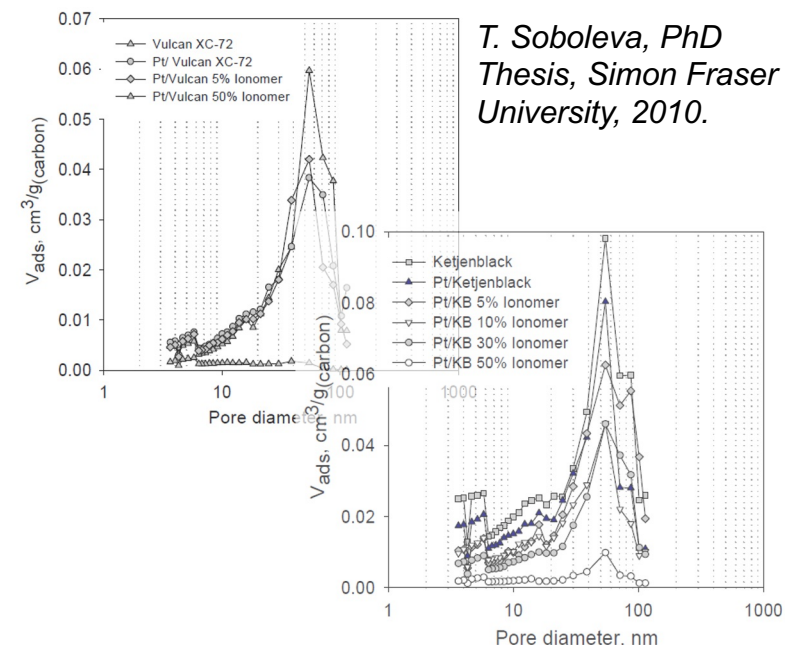
- ink composition (Pt:C, I:C)
- specific materials properties (support, catalyst, ionomer)
- dispersion medium
- fabrication conditions

CCL structure



~ 100 nm

- volume fractions (percolation)
- pore size distributions
- interface areas and properties
- wettability (distribution)
- ECSA, activity, and transport parameters



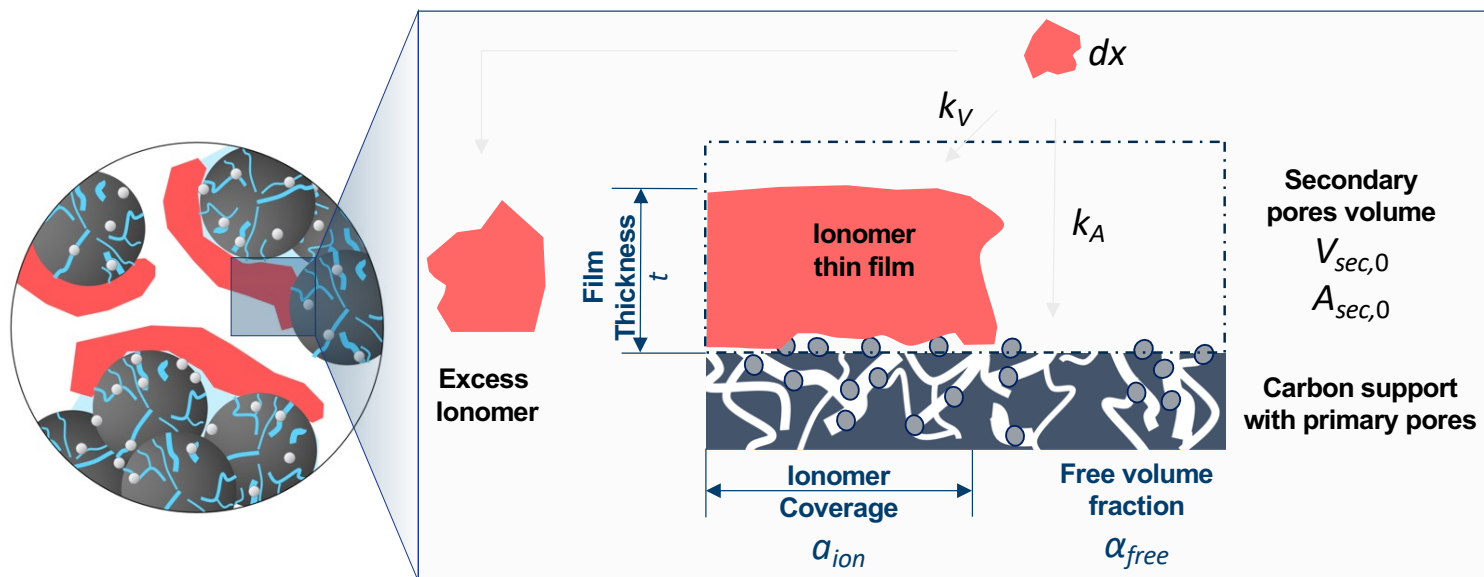
T. Soboleva, PhD
Thesis, Simon Fraser
University, 2010.

Example: evolution of pore size distribution and porosity

MODELING MICROSTRUCTURE FORMATION IN CCL

Prediction of volumetric composition and ionomer film thickness and coverage based on ink recipe

Model: Piecewise self-assembly of ionomer and carbon support during fabrication



Key parameter: ionomer dispersion parameter, k_A

$$x = \frac{V_{ion}}{V_{sec,0}}$$

$$d\alpha_{free} = -\alpha_{free} k_V dx$$

$$da_{Ion.} = (1 - a_{Ion.}) k_A dx$$

$$\alpha_{free} = \exp(-k_V x)$$

$$a_{Ion.} = 1 - \exp(-k_A x)$$

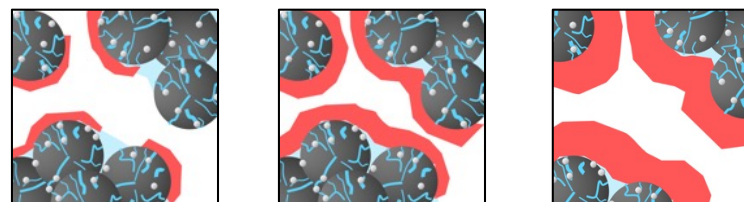
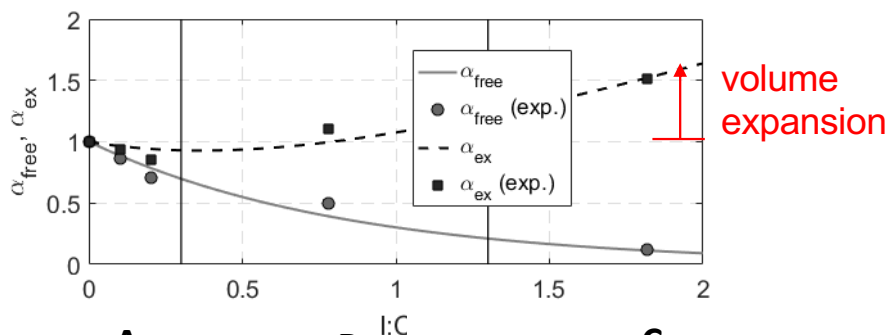
$$t = \frac{V_{sec,0}}{A_{sec,0}} \frac{1 - \exp(-k_V x)}{1 - \exp(-k_A x)}$$

$$V_{ex} = V_{sec,0} (x - \exp(-k_V x))$$

$$k_V = \frac{t_0 A_{sec,0}}{V_{sec,0}} k_A$$

MICROSTRUCTURE FORMATION MODEL: RESULTS

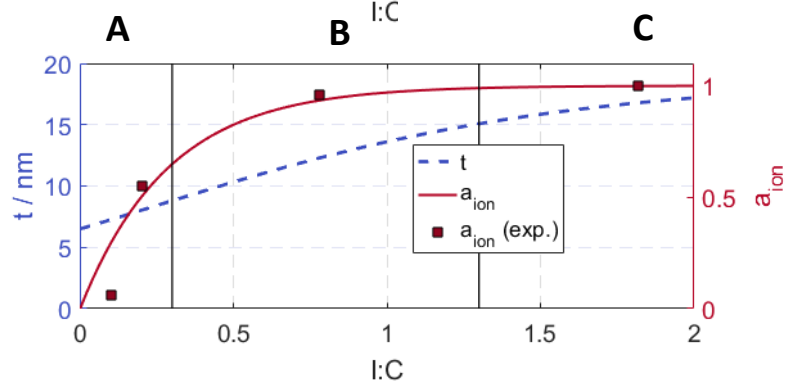
Basic correlations of ink parameters with CCL structure



A Coverage growth

B Film thickness growth

C Ionomer excess, CCL volume expansion



Exp. data: T. Soboleva., PhD thesis, Simon Fraser University, 2010.

W. Olbrich *et al.*, *Electrochim. Acta*, under review.



BOSCH



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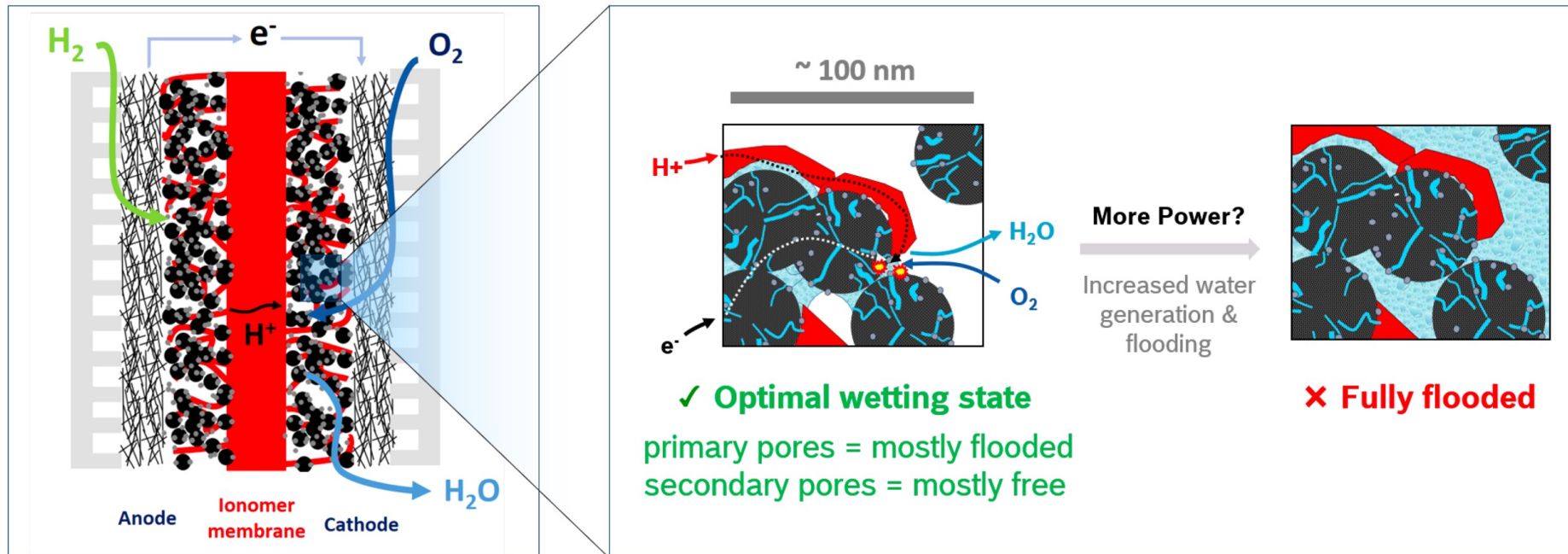
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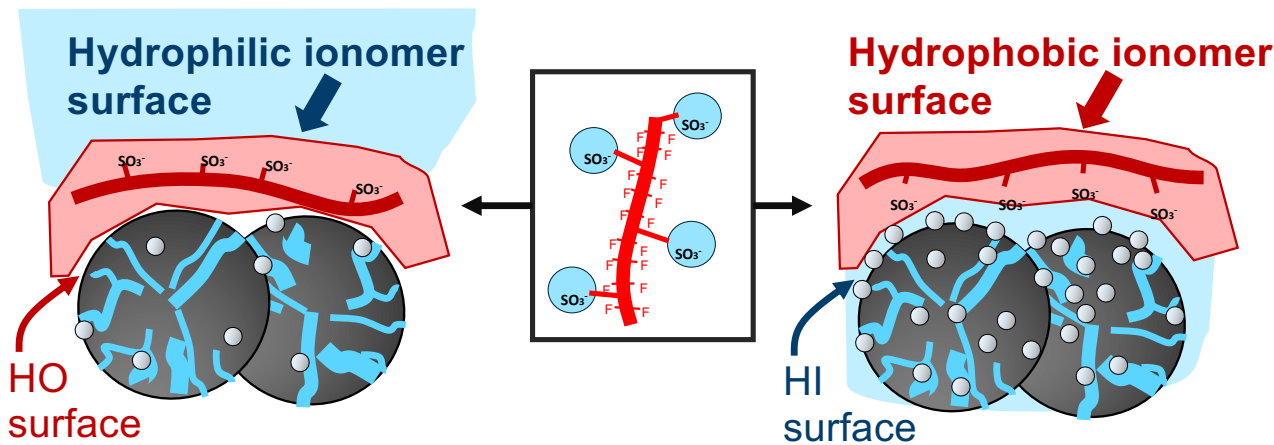
MODELING THE WETTABILITY DISTRIBUTION IN CCL

Water and flooding play a crucial role for CCL operation, especially at high current density



WETTABILITY MODEL: ROLE OF IONOMER

Orientation of ionomer sidechains is the key (surface-induced ionomer inversion effect)



→ quantitative analytical model

Journal of The Electrochemical Society, 2022 169 054521



Review—Wetting Phenomena in Catalyst Layers of PEM Fuel Cells: Novel Approaches for Modeling and Materials Research

W. Olbrich,^{1,2,3,4} T. Kadyk,^{1,4} U. Sauter,² and M. Eikerling^{1,3,4}

¹Theory and Computation of Energy Materials (IEK-13), Institute of Energy and Climate Research, Forschungszentrum Jülich GmbH, 52425 Jülich, Germany

²Robert Bosch GmbH, Corporate Research, 71272 Renningen, Germany

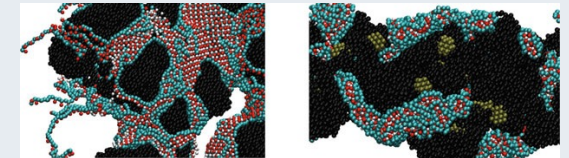
³Chair of Theory and Computation of Energy Materials, Faculty of Georesources and Materials Engineering, RWTH Aachen University, 52062 Aachen, Germany

⁴Jülich Aachen Research Alliance, JARA Energy, 52425 Jülich, Germany

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Ionomer inversion

□ earlier MD simulations



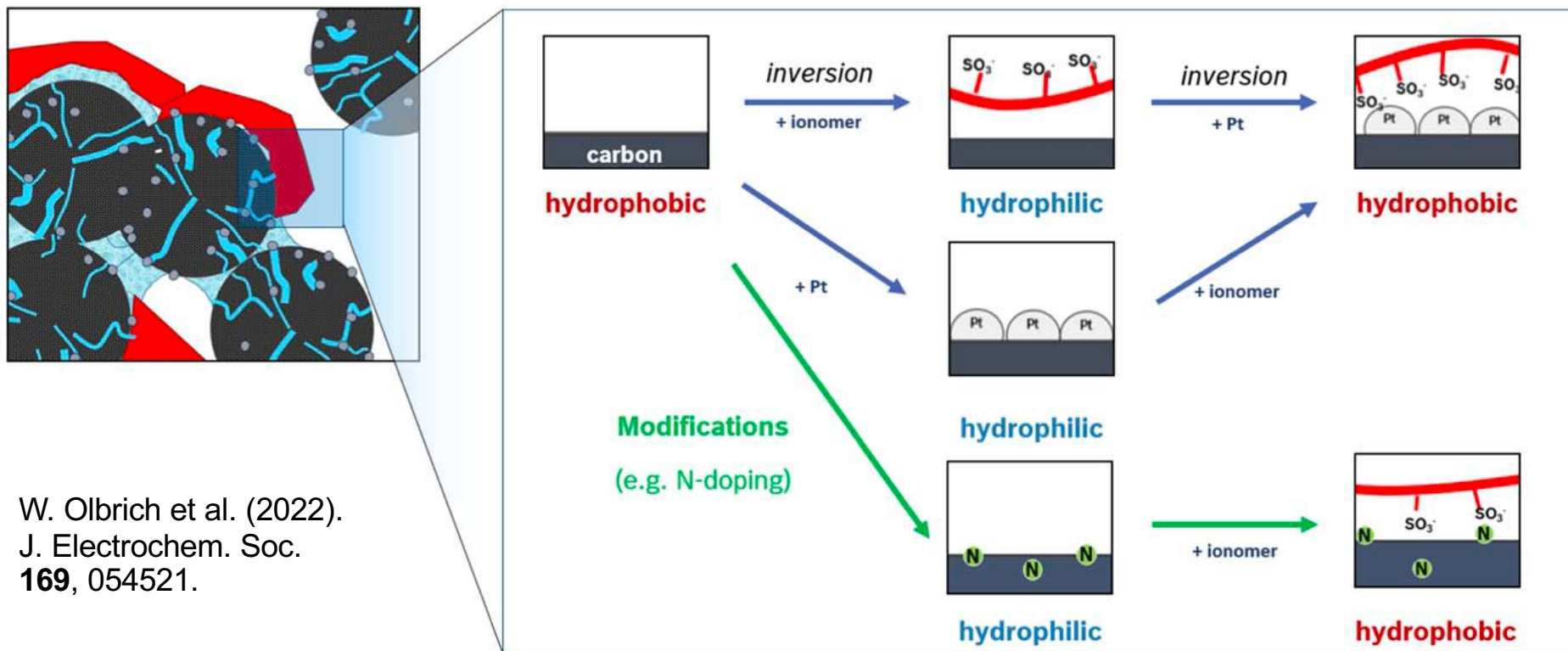
K. Malek *et al.* (2011).
Electrocatalysis **2**, 141-157.

□ experimental studies

Yu. M. Vol'fkovich *et al.* (2010).
Russ. J. Electrochem. **438**, 46.



INVERSION MECHANISM BASED ON VOL'FKOVICH DATA

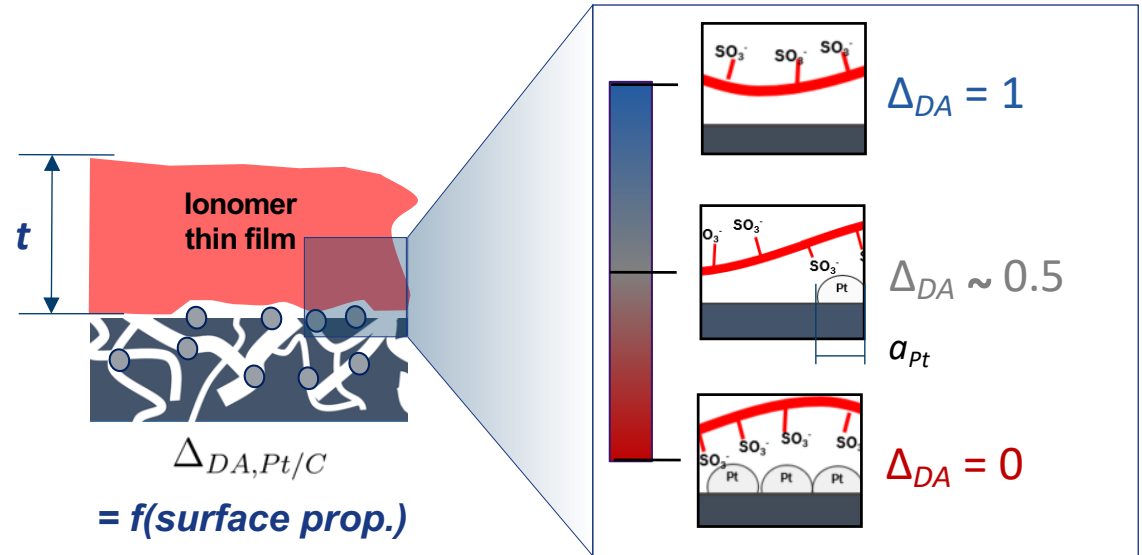


W. Olbrich et al. (2022).
J. Electrochem. Soc.
169, 054521.

WETTABILITY MODEL

Alignment of ionomer sidechains

- preferential ionomer sidechain orientation alters wettability in secondary pore space
- depends on chemical nature of surface and interaction with ionomer constituents
- Pt particles: help align sidechains towards support surface



Definition: degree of alignment, Δ_{DA} ,

$$\Delta_{DA} = 1 \Leftrightarrow \theta_{HI} = 30^\circ$$

$$\Delta_{DA} = 0 \Leftrightarrow \theta_{HO} = 120^\circ$$

$$\Delta_{DA, \infty} \sim 1/3 \Leftrightarrow \theta_{\infty} \sim 90^\circ$$

$$\Delta_{DA, Pt/C} = \Delta_{DA, C}(1 - a_{Pt}) + \Delta_{DA, Pt} a_{Pt}$$

$$\Delta_{DA}(t) = \Delta_{DA, \infty} + (\Delta_{DA, Pt/C} - \Delta_{DA, \infty}) \exp\left(1 - \frac{t}{t_0}\right)$$

$$\cos(\theta_{ion}) = \Delta_{DA}(\cos(\theta_{HI}) - \cos(\theta_{HO})) + \cos(\theta_{HO})$$

$$\cos(\theta_{sec}) = a_{ion} \cos(\theta_{ion}) + (1 - a_{ion}) \cos(\theta_{Pt/C})$$

WETTABILITY MODEL

Stochastic process to generate heterogeneously wetted surfaces

- ionomer (chunks of fixed size, $r_{ion} \sim 5$ nm) distributed randomly
- normal distributions based on mean and variance of (n,p)

binomial process:

$$p = a_{ion}$$

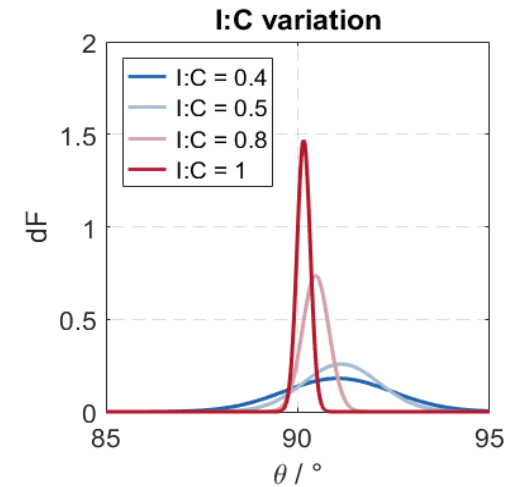
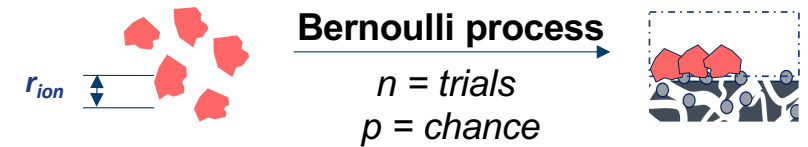
$$n = k_{max} = \frac{A_{pore}}{A_{ion}} = f(r_{pore}^2)$$

$$n \gg 1$$

$$\mu_k = k_{max} a_{ion}, \sigma_k^2 = k_{max} a_{ion} (1 - a_{ion})$$

Obtain water retention curve by integration over pore size distribution (PSD), contact angle distribution (CAD) and Young-Laplace criterion (YLP):

$$S(p_C) = \int_{r_{min}}^{r_{max}} \int_{-1}^1 PSD(r) \cdot CAD(r, \cos(\theta)) \cdot YLP(r, \cos(\theta), p_C) d \cos(\theta) dr$$

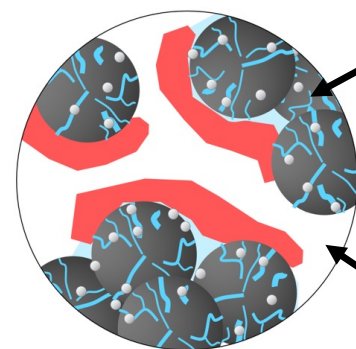
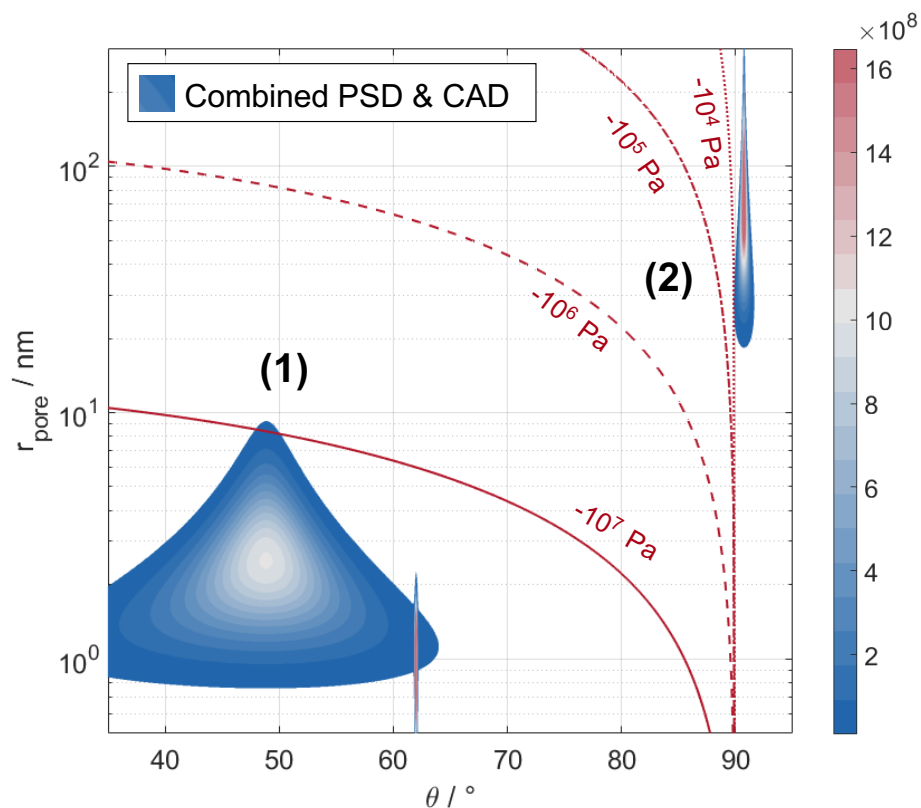


Origin of mixed wettability!



WETTABILITY MODEL: RESULTS

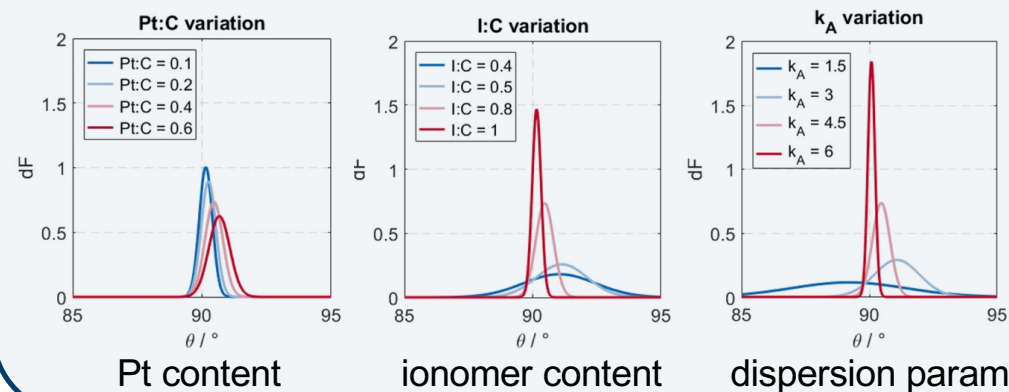
Pore size and contact angle distribution



(1) Hydrophilic primary pores and Pt-free nanopores

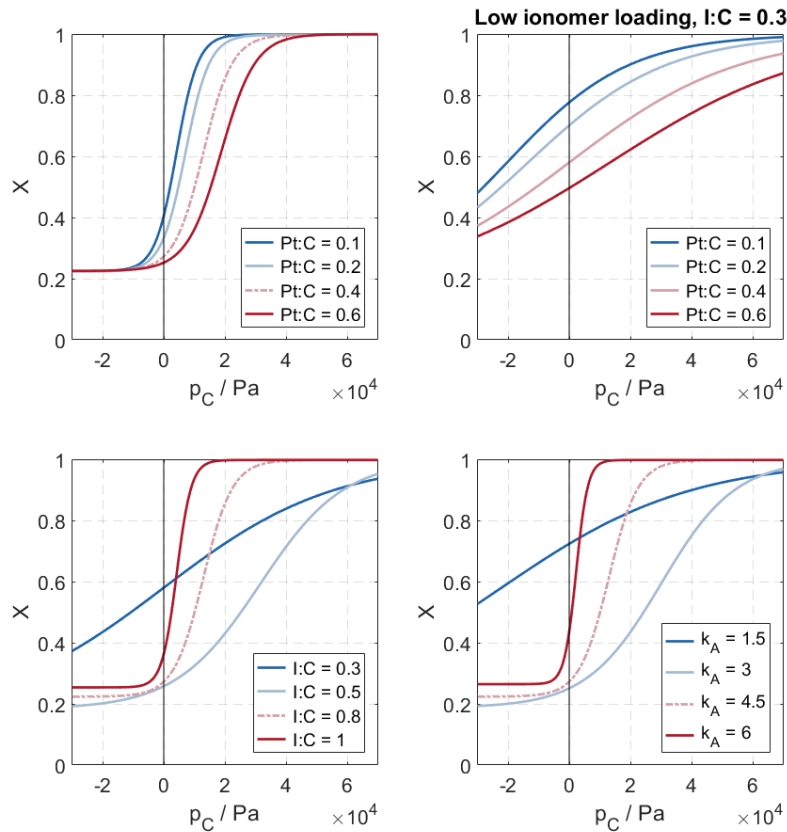
(2) Secondary pores with mixed wettability

Contact angle distribution (secondary pores)

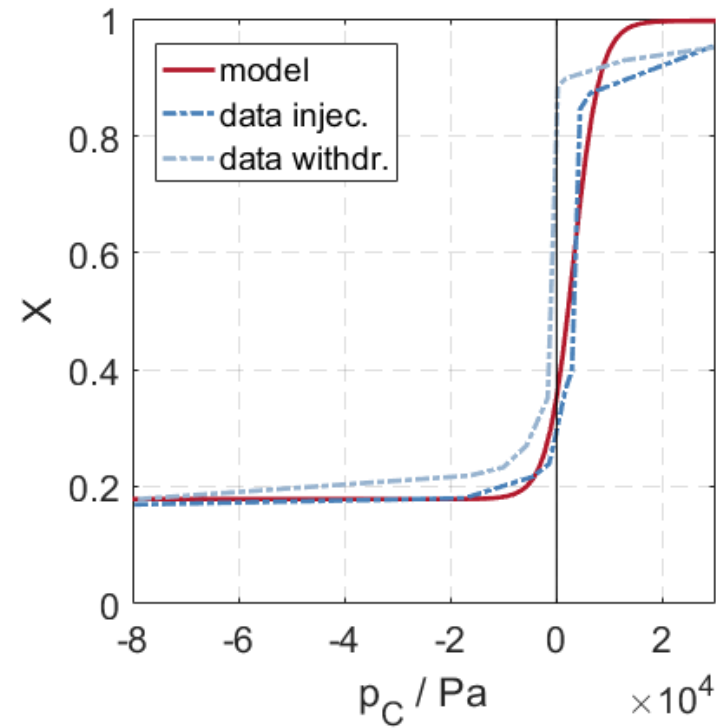


WETTABILITY MODEL: WATER RETENTION CURVES

Parametric effects



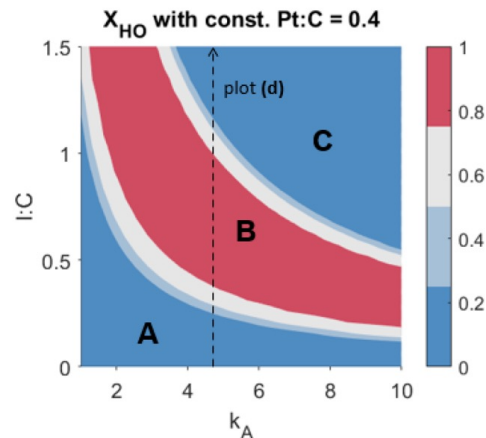
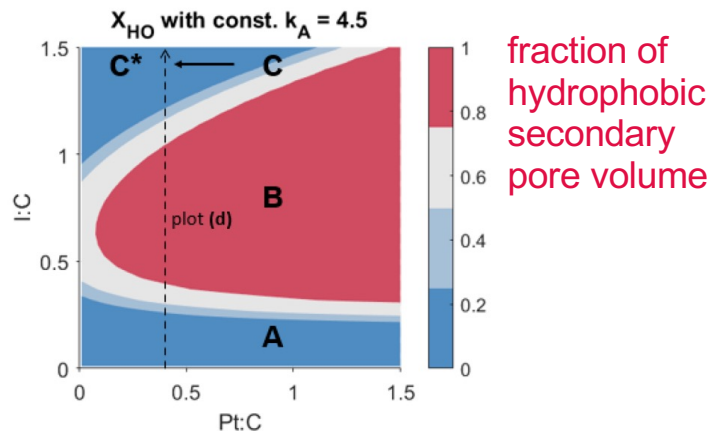
Comparison to experiment



H. P. F. Gunterman,
PhD thesis, UC
Berkeley, 2011.

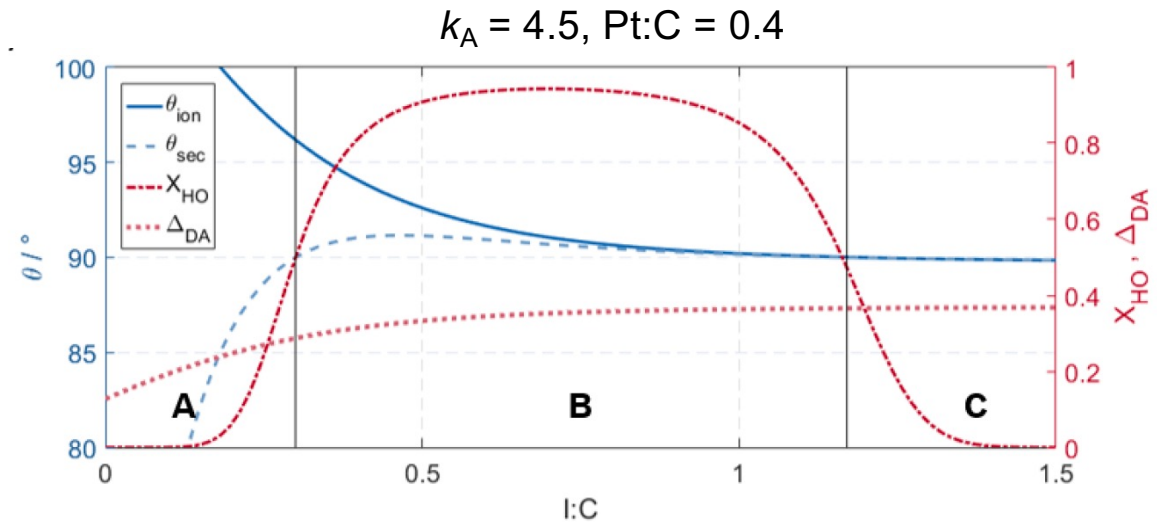
WETTABILITY MODEL: CCL OPTIMIZATION

Materials selection, modification, and design: tune parameters for optimal wettability distribution



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W. Olbrich *et al.*, *Electrochim. Acta*, under review.

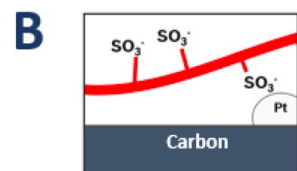
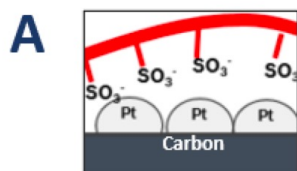
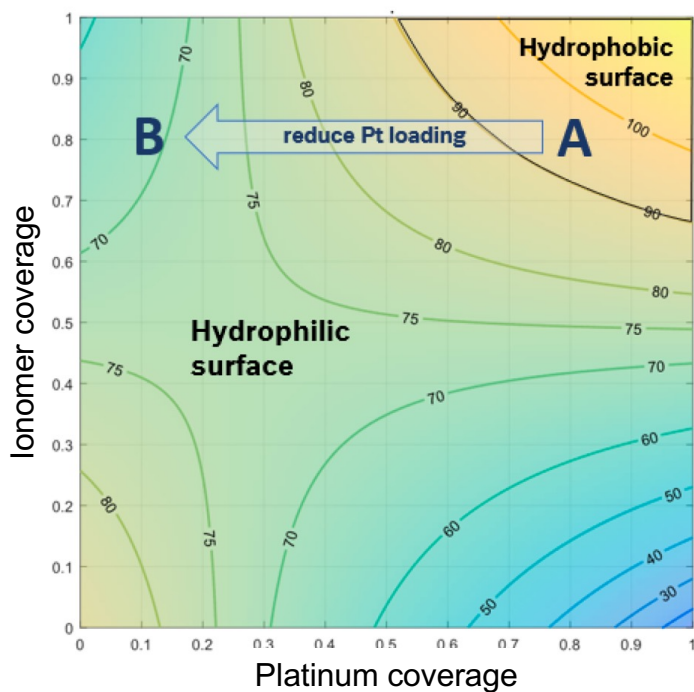


- ❑ reducing Pt loading can tip the water balance (as seen earlier)
- ❑ lower Pt loading: ionomer content must be more finely tuned
- ❑ support modification: less sensitive to Pt and ionomer loading

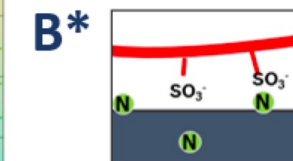
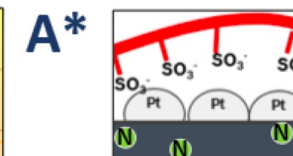
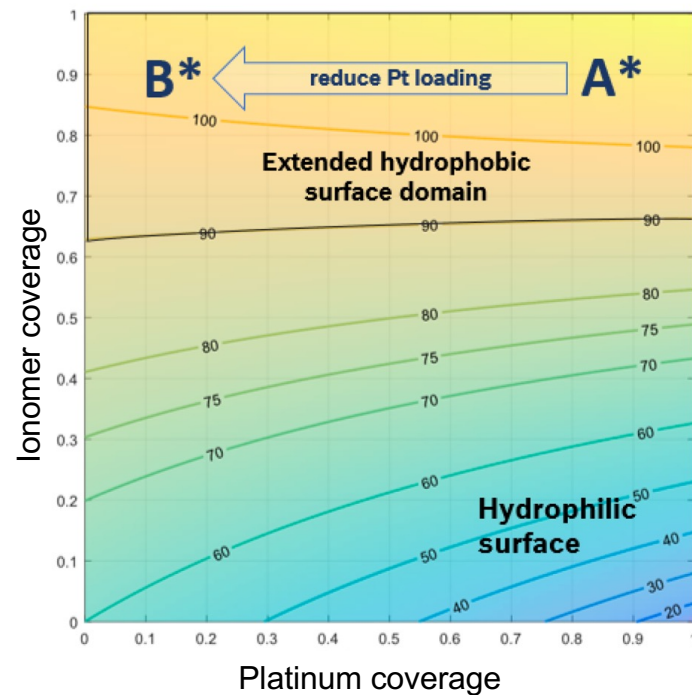
WETTABILITY MODEL: SUPPORT MODIFICATION

Effective contact angle of Pt/C/ionomer composite

conventional carbon support



functionalized carbon support



W. Olbrich et al. (2022). J. Electrochem. Soc. **169**, 054521.

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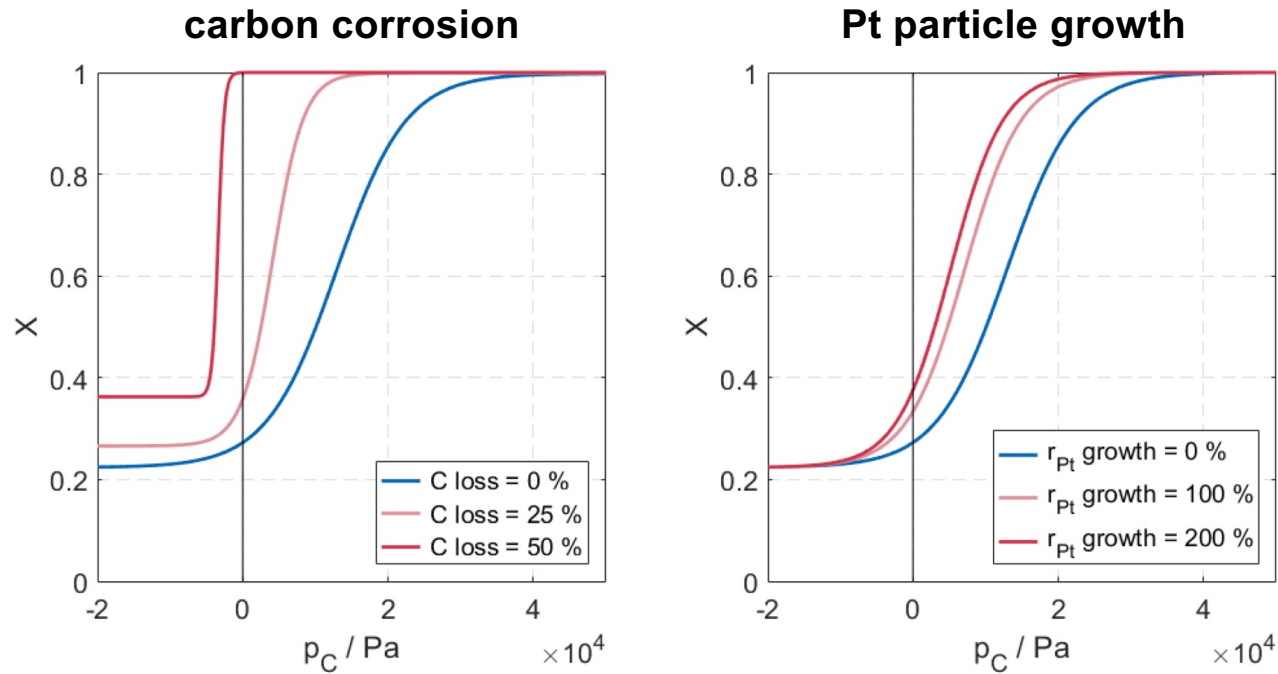


Michael Eikerling, IEK-13: Theory and Computation of Energy Materials

m.eikerling@fz-juelich.de

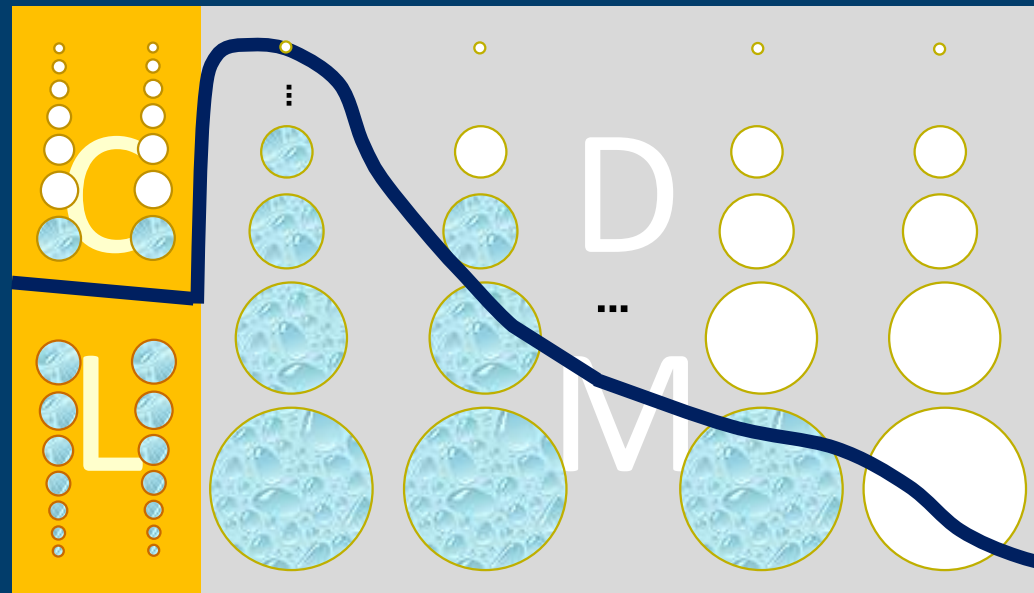
WETTABILITY MODEL: DEGRADATION EFFECTS

Changes in wettability and water retention behaviour during lifetime



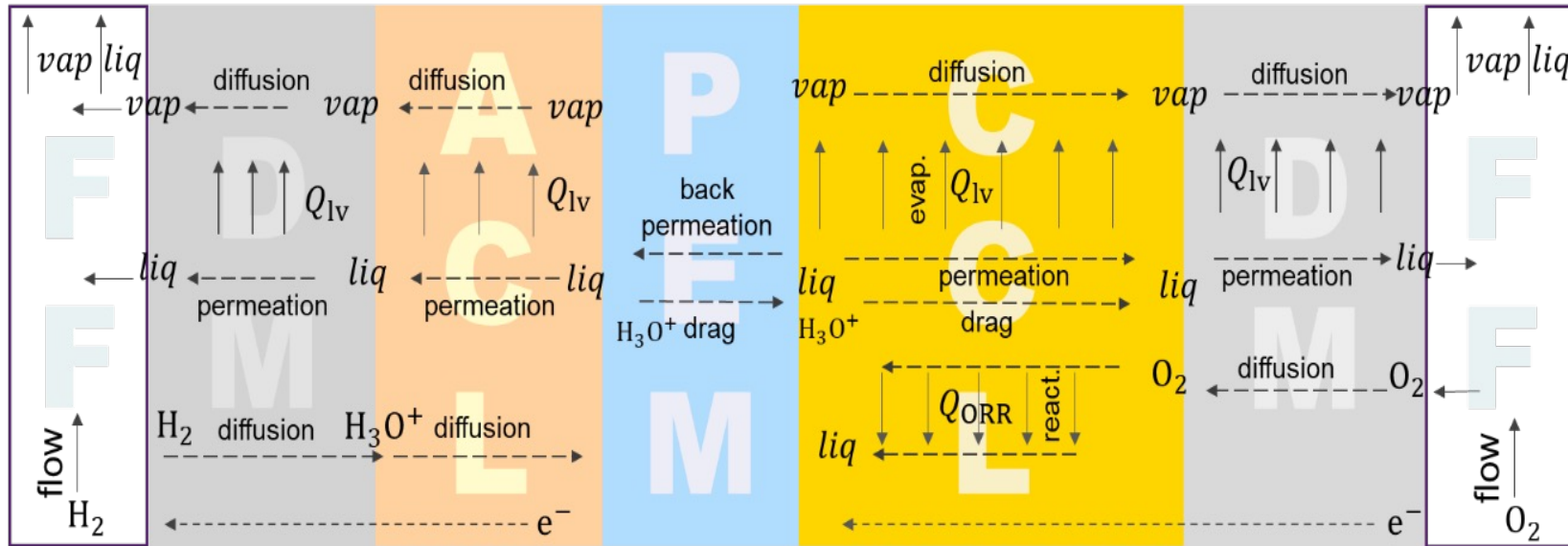
Shifting the tipping point

DEVELOPING STORY: MODELING LIQUID WATER ACCUMULATION IN PEM FUEL CELL CATHODE



ACCOUNT FOR CROSS COMPONENT COUPLING

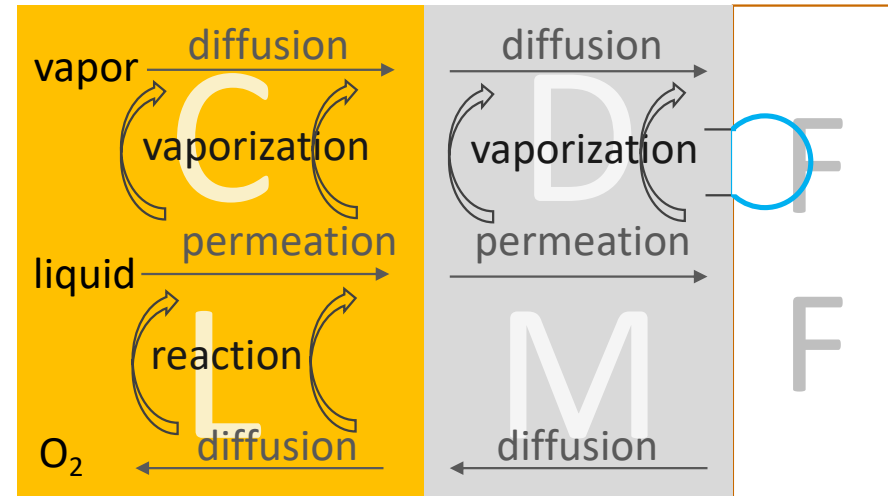
Comprehensive model for water balance in cathode CL and DM



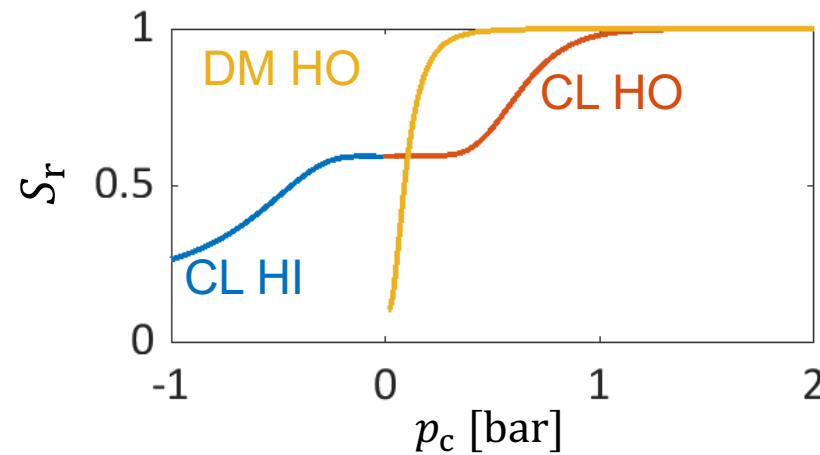
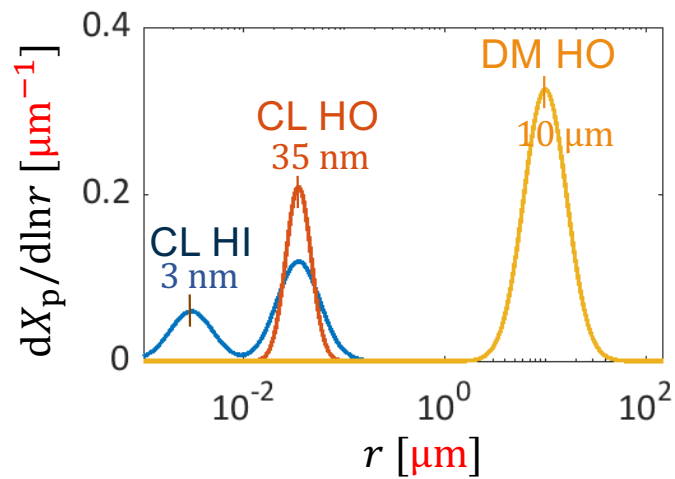
Solution space: pressure distribution → liquid saturation, fluxes

MODEL ASSUMPTIONS

- ❑ cathode side: CL & DM and DM-FF interface
- ❑ transport of oxygen (air), liquid and vapor water
- ❑ one-dimensional
- ❑ macrohomogeneous
- ❑ isothermal

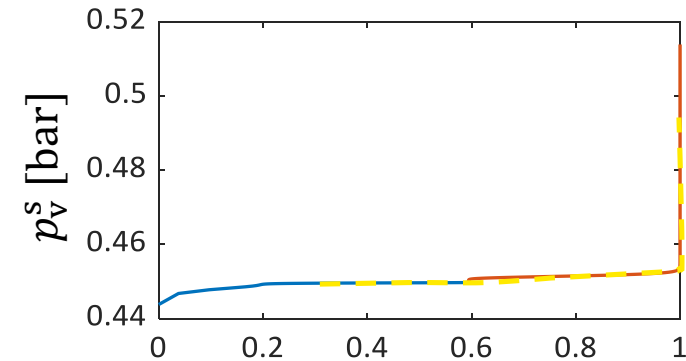
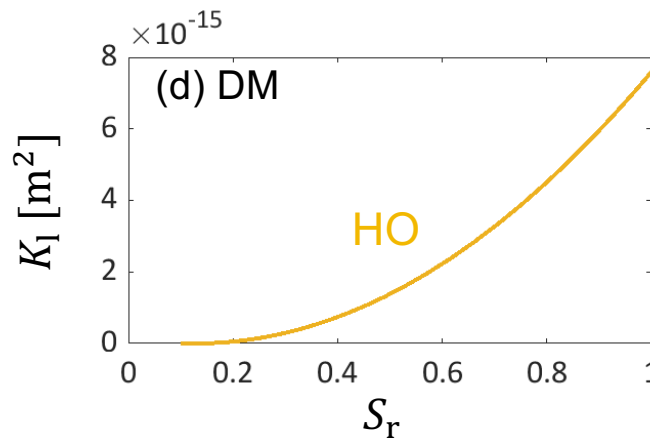
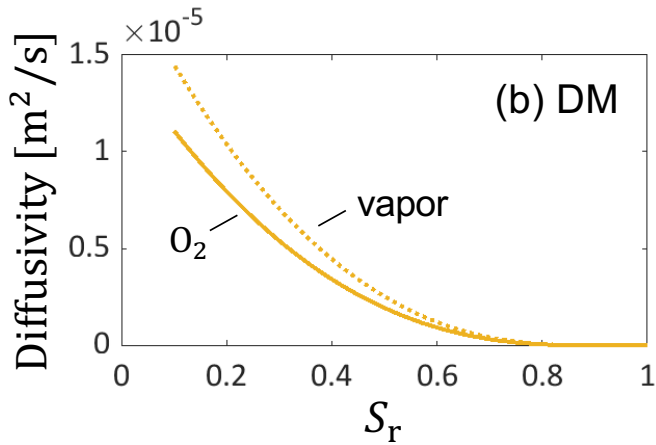
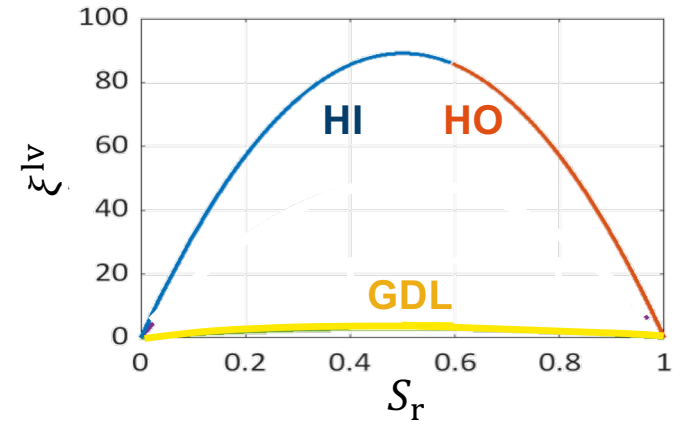
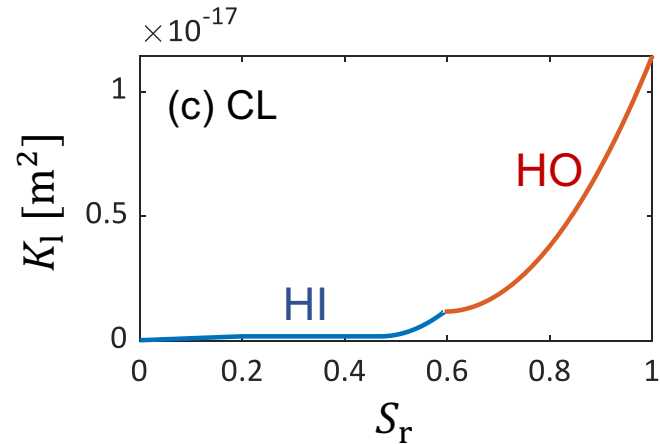
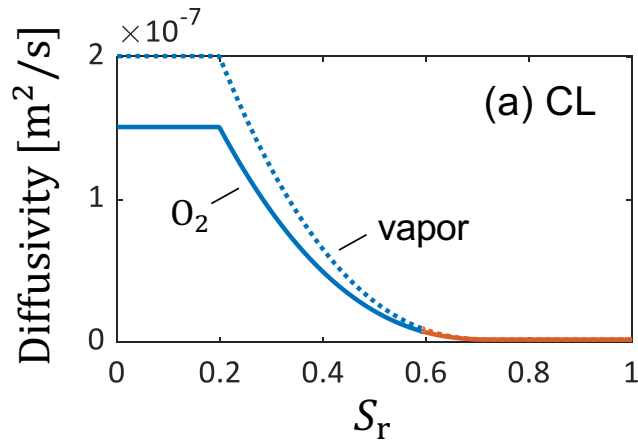


PORE SIZE DISTRIBUTIONS AND WATER RETENTION CURVES



At the same p_c , S_r in **CL** and in **DM** are different.

EFFECTIVE PROPERTIES AS FUNCTION OF LIQUID SAT



DIFFERENTIAL EQUATIONS AND BOUNDARY CONDITIONS

Left Boundary

CL

Middle Boundary

DM

Right Boundary

P
E
M

$$J_{O_2} = 0$$

$$J_v = 0$$

$$J_1 = 0$$

Transport equations

$$J \propto -D \nabla c$$

$$J \propto -K \nabla p$$

Continuity equations

$$\frac{dc}{dt} + \nabla \cdot J = \sigma$$

$$\frac{dJ_1}{dx} = -2\sigma_{O_2} - \sigma_v$$

$$p_{O_2} = p_{O_2}$$

$$J_{O_2} = J_{O_2}$$

$$p_v = p_v$$

$$J_v = J_v$$

$$p_1 = p_1$$

$$J_1 = J_1$$

$$\frac{dp_{O_2}}{dx} = -\frac{RT}{D_{O_2}} J_{O_2}$$

$$\frac{dJ_{O_2}}{dx} = 0$$

$$\frac{dp_v}{dx} = -\frac{RT}{D_v} J_v$$

$$\frac{dJ_v}{dx} = \sigma_v$$

$$\frac{dp_1}{dx} = -\frac{V\mu}{K_1} J_1$$

$$\frac{dJ_1}{dx} = -\sigma_v$$

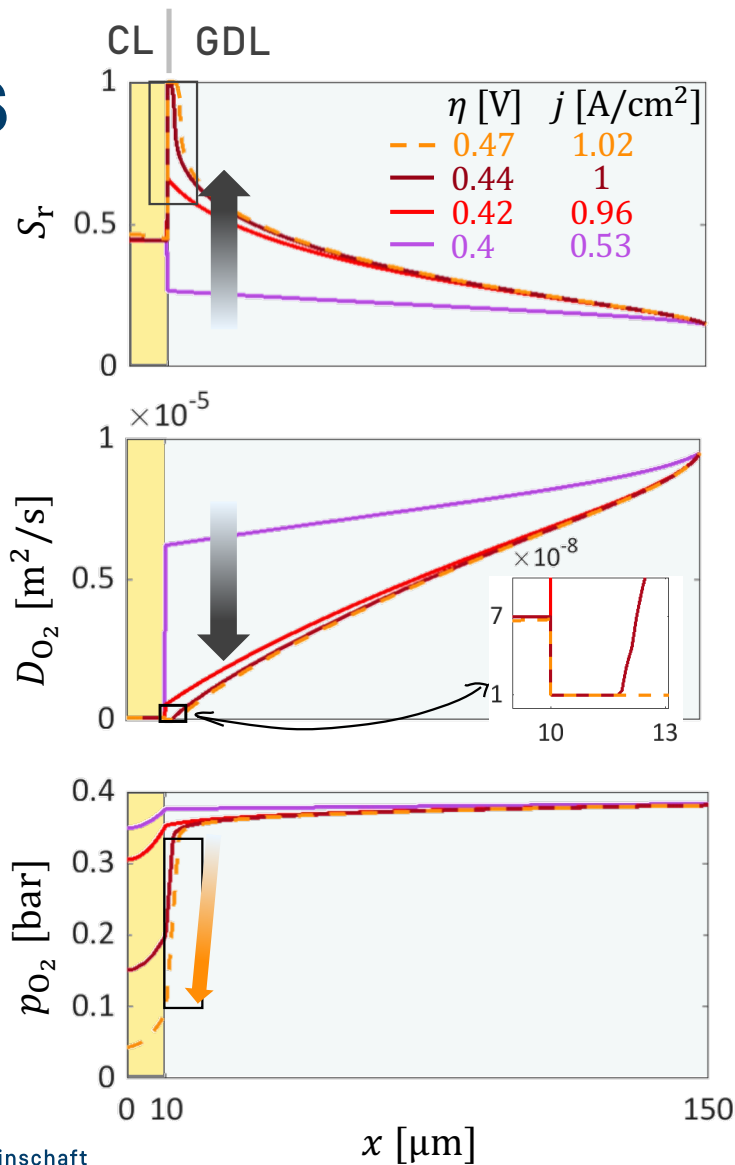
$$p_{O_2} = p_{O_2}^{\text{in}}$$

$$p_v = p_v^s \times RH$$

$$p_1 = p_g + p_c^{\text{DM-FF}}$$

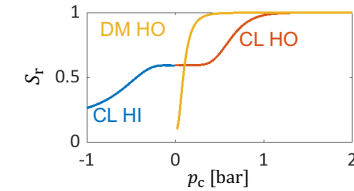
F
F

RESULTS



Liquid saturation:

- does not change much in CCL with j
- GDL: formation of water layer at CL|GDL above j_c

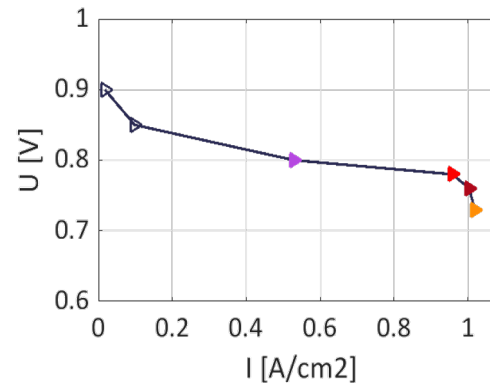


O₂ diffusivity:

- water layer causes abrupt decrease in diffusivity (to residual value)

O₂ partial pressure:

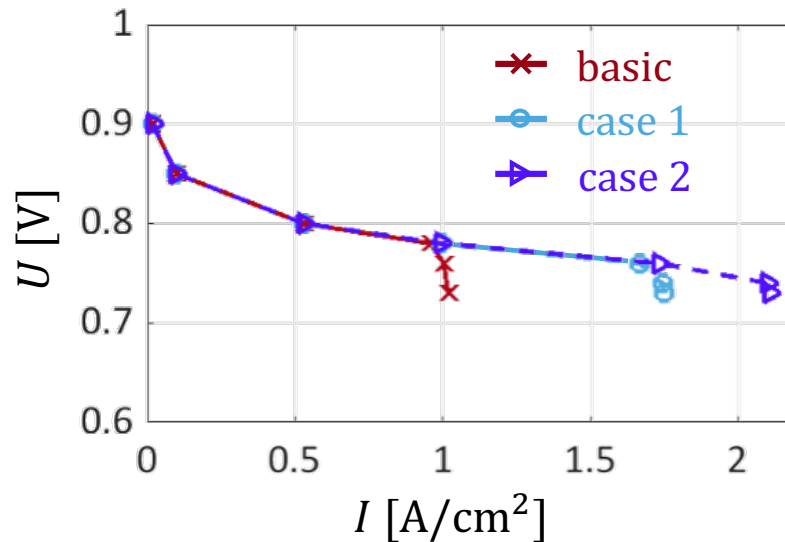
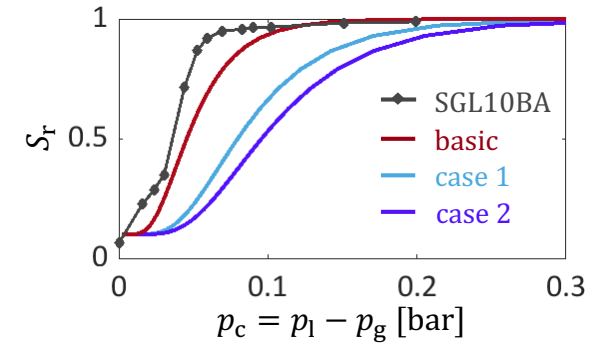
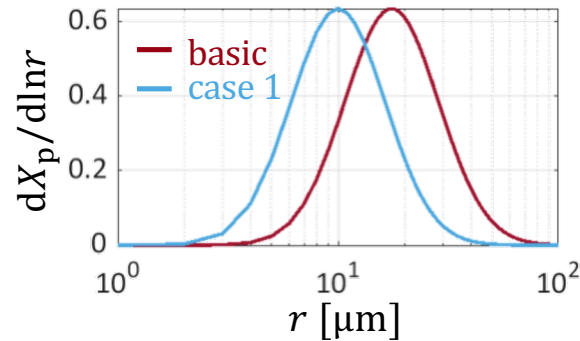
- drops drastically above j_c before even reaching the CCL



HOW TO SUPPRESS WATER LAYER FORMATION?

Tune the water retention curve: pore size distribution or contact angle

	basic	case 1	case 2
$r_{\text{GDL}} [\mu\text{m}]$	17.5	10	17.5
$\theta_{\text{GDL}} [^\circ]$	133	133	145



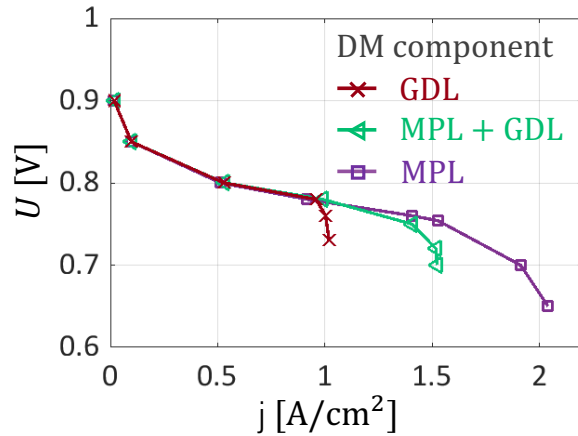
Strategies

- smaller HO pores
- larger contact angle

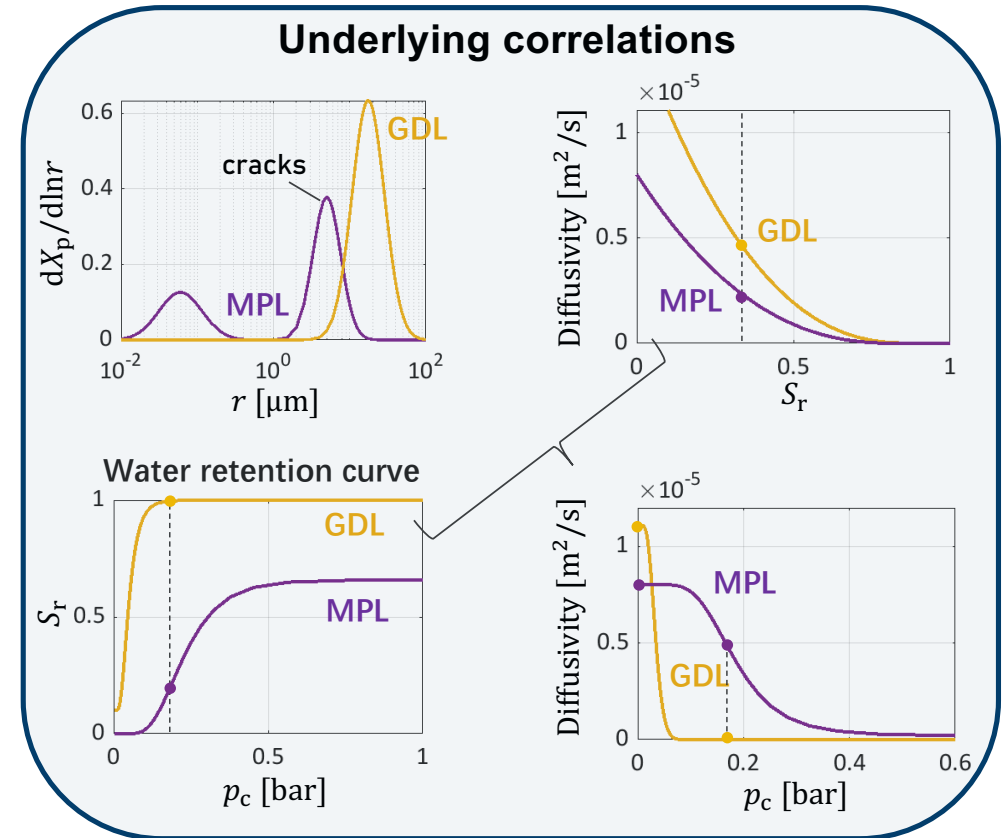
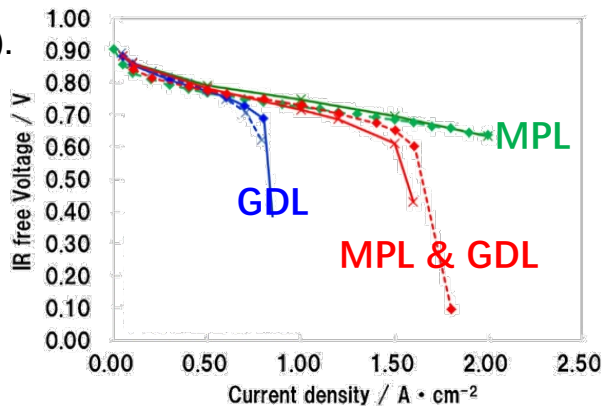
Water retention curve matters!

HOW TO SUPPRESS WATER LAYER FORMATION?

Introducing another porous layer, the MPL!



K. Totaka et al. (2014).
ECS Trans. **64**, 839.



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Michael Eikerling, IEK-13: Theory and Computation of Energy Materials

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SUMMARY

Physical modeling as starting point for correlation analysis (j - V data)

Making sense of extensive performance data for Pt loading reduction

Role of ionomer: control local pH (and conductivity) and wettability

Model of structure formation (ionomer assembly in catalyst layer)

Learn how to keep secondary pore space hydrophobic

Learn how to suppress water layer formation at CL|GDL boundary